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SPECKLEGRAM DATA REDUCTION USING OPTICAL AND DIGITAL TECHNIQUES--ETC(U)
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SPECKLEGRAM DATA REDUCTION USING OPTICAL AND DIGITAL TECHNIQUES

Electro-Optics Technology Branch
Electronic Technology Division

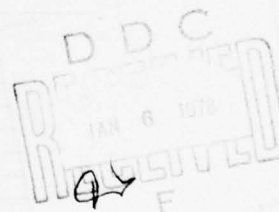
November 1977

TECHNICAL REPORT AFAL-TR-77-203

Final Report for Period May 1974 to September 1976

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AIR FORCE AVIONICS LABORATORY
AIR FORCE WRIGHT AERONAUTICAL LABORATORIES
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This technical report has been reviewed and is approved for publication.

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report describes the development of a specklegram data reduction system for automatically analyzing specklegram output. The basic design incorporates a PDP-11 minicomputer as an overall control center with various optical and electronic components interfaced to the computer. Typical data runs yielded 1-2 second turn around time for each specklegram data point and approximately 1-2 fringe resolution over a specific output halo.		

FOREWORD

The major goal of this program is the development of a breadboard in-house laboratory measurement system. In pursuing this objective many experimental results were obtained which shed light on some improvements that could be made toward further development of such a system. These results are presented in this report along with some tried designs and proposed designs. The system was designed to readout specklegram data and display the information in a readable format with an automated optical-digital set-up, thus reducing the analysis time greatly over existing methods. The overall system design and end results are discussed in this report, which will be a final report to the Air Force Flight Dynamics Laboratory under project 1367-02-12. Mr. Gene Maddux and Dr. Frank Adams were the scientific contacts from AFFDL.

I would like to thank Dave Flannery of AFAL/DHO-2 and Chuck Skinn of System Research Lab. for their assistance in pursuing these Program goals.

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SECTION I

INTRODUCTION

Near the beginning of FY74 Gene Maddux and Dr. Frank Adams of the Air Force Flight Dynamics Laboratory visited Tom Williamson and Dick Lane of the Air Force Avionics Laboratory seeking a feasible method for analyzing specklegram data with a semi-automated optical data processing system. A set-up, made up of existing in-house equipment including a desk calculator, digital voltmeter A/D converter, and a motor driven scanning detector, was constructed immediately in the Laboratory of Bldg 22B and after several test conclusions indicated that an optical processing system could be fabricated to meet the requirements of AFFDL. (A copy of the initial study is attached at the end of the report.)

In January 1974 Dr. Adams requested and obtained \$24,000 of AFFDL Laboratory Director's Funding (LDF-74-1) to finance a joint program with AFAL for developing an automated data readout and reduction technique for laser speckle photography. AFFDL funding was used to procure equipment and AFAL provided the engineering manpower.

A plane of attack was then begun for which the following equipment was ordered at the beginning of FY75: Minicomputer, X-Y Translation Stage, 2 dimensional detector, A/D convertor, clocking circuit. The final delivery of equipment was received in May of 1975 and the fabrication was underway. This report gives the demonstration of the brassboard optical-digital system fabrication for performing data reduction of specklegram recordings.

SECTION II

STATEMENT OF PROBLEM

In the early 1970s several researchers in the United Kingdom showed that small in-plane displacement measurements could be made by using the inherent speckle properties of laser light and employing double exposure photography (References 1 to 6). Further development of this technique, called "Speckle Photography," has been pursued at the Air Force Flight Dynamics Laboratory (References 7 to 11). It was found that the speckle distribution change during stressed and unstressed conditions on specified surfaces gives a direct indication of the amount of surface motion present under stress. This recording process is performed with a single beam laser imaging system, and as many as 40,000 data points can be recorded on a 4 inch by 5 inch photographic plate with one double exposure. At this point it was realized that to use the high resolution recording to its utmost, a readout system had to be established to speed up the method for extracting the data in its entirety. The laboratory readout method used originally consisted of projecting the output fringes on a ground glass screen, then orienting a slow scanning detector orthogonal to the fringe lines, and scanning the detector while plotting directly onto an x-y recorder. This process has to be performed for each data point on a specklegram plate with the addition of one accurate method for scanning from data point to data point. The average point to point recording time could be as large as 5 minutes, thus requiring 140 hours to analyze a single plate.

Careful study has shown that to establish the speckle photography method as a feasible tool for performing non-destructive testing, the point to point data collection time, including the point to point scan time, must be 1 second or faster. At these rates, the maximum time required to read a specklegram plate at maximum resolution would be 1.5 hours. A faster time can be achieved with some modifications to the existing brassboard described in this report. The modifications are discussed in the section entitled "Conclusions with Alternate Solutions."

The problem of data reduction of specklegram output appears to be solvable by a digital-optical system, and with further experimentation, a time improvement and resolution improvement are realizable over the initial brassboard setup.

SECTION III

DESCRIPTION OF OPTICAL SETUP

Figure 1 is a graphical illustration of the optical section of the brassboard system used for reading out specklegram data provided by the Flight Dynamics Laboratory for experimental use. A Spectra Physics Model 124-A He-Ne Laser with 15 milliwatts of power and a 1 millimeter diameter beam is the light source for the system.

Two lenses with a 4 to 1 focal length ratio are required to reduce the laser beam diameter to its optimal operating size. Microscope objectives of 20 power and 5 power were chosen for this experiment. The lenses are oriented such that the distances between them equals $f_{20} + f_5$, thus the 1 mm collimated beam emerging from the laser enters the specklegram plate at .25 millimeters. A .25 millimeter beam was chosen because experimentation showed that a smaller beam would create large secondary speckle and a larger beam would reduce the inherent resolution of a data plate.

The specklegram plate is held in a plate holder attached to a 5 inch by 5 inch Yosemite x-y translation stage (Figure 2). The stage, with .0001 inch stepping resolution, mechanically positions the data plate to each new data point position, with two Slo-Syn stepping motors tied directly to the worm gear mechanism on the stage. Each step of rotation by the motors represents a .001 inch lateral motion of the stage and is controlled by the PDP-11 central processor tied to a specially built electronic circuit constructed in-house by AFAL. The details of the central processor software and control circuit are described in two later sections of this report.

A ground glass plate, ground with 10 micron Carborundum, serves as a projection screen from which the specklegram fringes are imaged. The ground glass screen can be vibrated as a means of reducing the unwanted secondary speckle noise. An opaque 1/2 inch diameter spot is placed

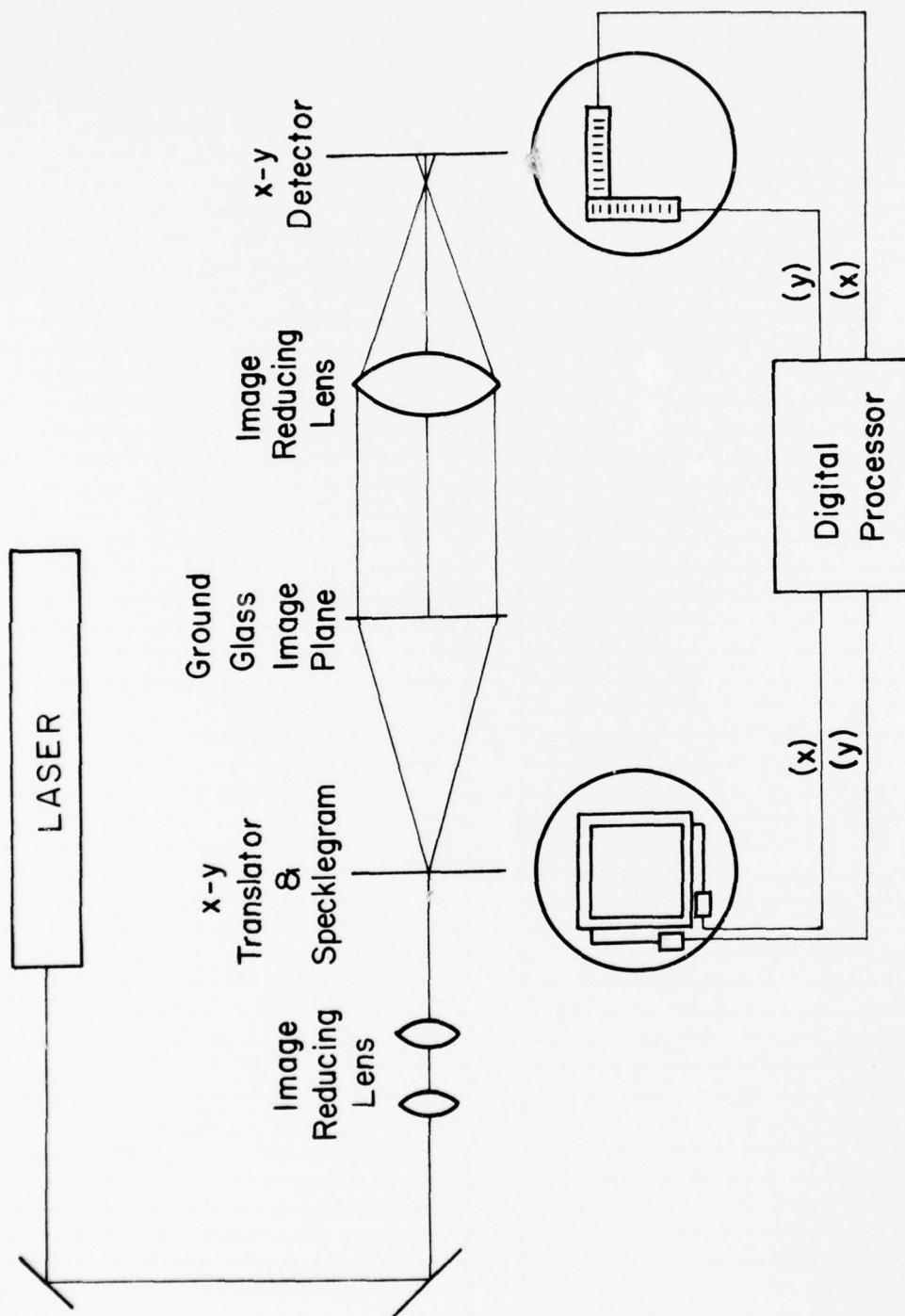


Figure 1. Graphical Description of Optical Setup



Figure 2. X-Y Stepping Stage

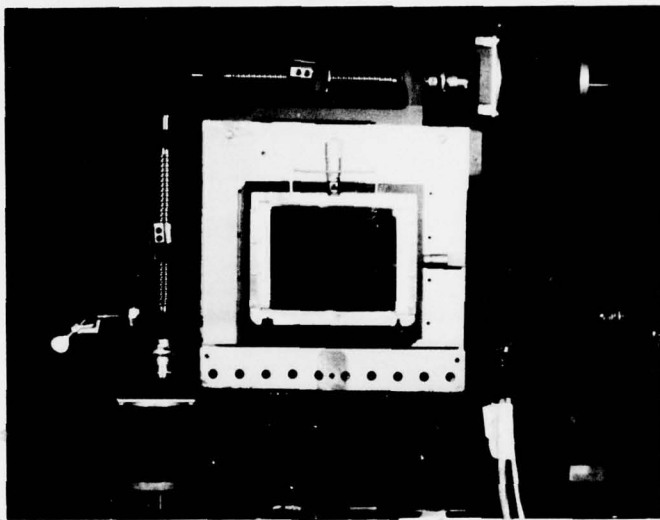
on the ground glass at the center of the speckle pattern canceling the D.C. component of the readout beam, in order to avoid detector saturation at the D.C. imaging point.

The primary speckle size used in constructing a specklegram determines the projection cone angle of the fringe pattern; thus as a ground glass screen is moved further from a specklegram the fringe size increases as the area of a plane, subtending a cone perpendicular to the cone axis. When sizing the secondary speckle to match the ground glass screen consistency, a hole of about six inches in diameter is optimal; thus an image reducing lens is required to project the proper fringe size onto the orthogonal detector assembly. A vivitar 28 Millimeter focal length lens is used for the brassboard system being described. Since specklegrams, as stress analysis tools, are produced with different imaging systems, varying reconstruction cone angles dictate that the optical geometry between the specklegram and detector

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FIG-2

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be variable. The ground glass screen and the detector assembly are positioned by two micrometer controlled slide stages.

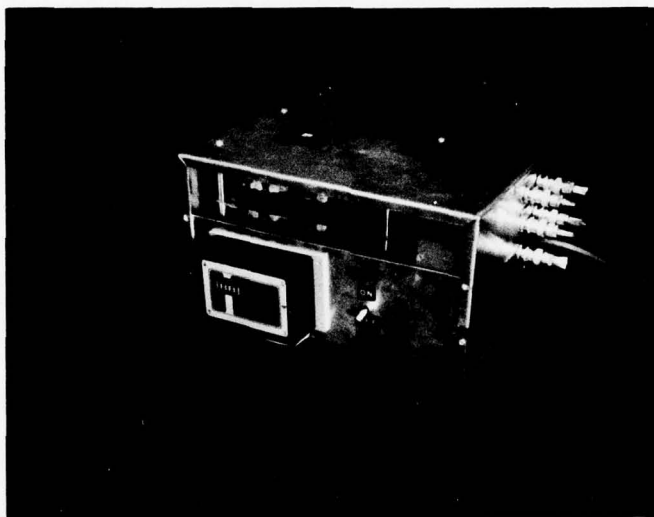
Fulfilling the need for a medium to pick up the imaged fringe data is a custom built detector system consisting of two linear detector arrays and associated operating circuits (Figure 3). Appendix V gives a detailed description of the specification and operating procedures of a Reticon Corporation Detector System similar to the RL-64 WP Model incorporated in the optical setup. The circuitry for operating the detector consists of five main electronic sections: 1.) - 2.) Output drivers; 3.) Clocking circuit; 4.) - 5.) Sample and hold circuits. The output drivers, required for each linear array, simply amplify the output signal from each detector in the array to a 3 volt maximum during the light saturation operation. The amount of light required to reach saturation is obviously dependent on the length of time the detector is receiving light and, since the detectors integrated



Figure 3. Reticon Detector

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FIG-3

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all the incident light from one reading to the next, the scan time from detector to detector determines the optical saturation level. The clocking circuit which controls both detectors has a direct influence on the detector to detector read time. A more detailed description of the electronic circuit sequencing will be discussed in Section IV, 3. Circuits 4 and 5 are merely sample and hold electronics that read the output from the driver circuits and retain them for a time period long enough for an external readout. For instance, if the signal illustrated in Figure 4b were input to the sample and hold board it would emerge as shown in Figure 4a. In other words, a series of spiked pulses is transformed into a series of square wave pulses. At this point attention will be given to the configuration of the linear detector element relative to the optical fringe output. Figure 5 is a magnified view of the two linear detector arrays configured in a chip holder. The particular geometry chosen will allow the specklegram fringes to be projected onto the detector array at any angle but will make it still possible to determine the orthogonal spacing between fringes. By looking at Figure 6, we see that if the x and y axis represent the two linear detector arrays and the three skewed lines represent the fringe data, a simple trigonometric sequence allows us to determine the orthogonal spacing (d) and the fringe angle placement (θ) from the fringe spacing which appears on the detector arrays (x and y). The trigonometric sequence is as follows:

$$\begin{aligned}\theta &= \tan^{-1} y/x \\ d &= x \sin \theta \\ d &= x \sin (\tan^{-1} y/x) \\ d &= xy / \sqrt{y^2 + x^2} \\ d &= x / \sqrt{1 + (x^2/y^2)}\end{aligned}$$

Thus, by employing two linear detector arrays set in a right angle field, a complete set of useful data can be extracted from any specklegram plate. The original detectors purchased from Reticon Corporation were 64 elements long, and since a maximum of 20 fringes

would ever enter the system, the Sampling Theory says 64 elements would suffice. But, it has been determined through experimentation that this number is too low to perform the job as accurately as required.



Figure 4. Reticon Output Samples



Figure 5. Magnified View of the Reticon Detectors Elements

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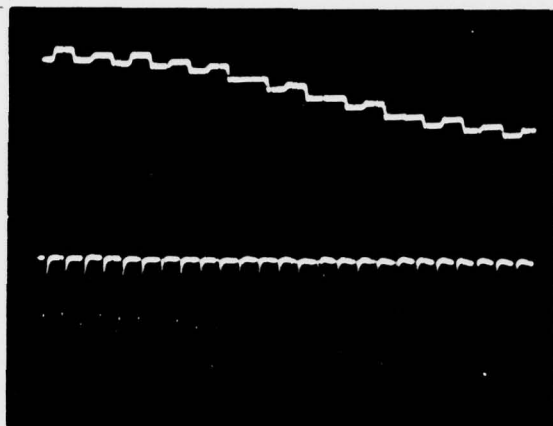


FIG-4

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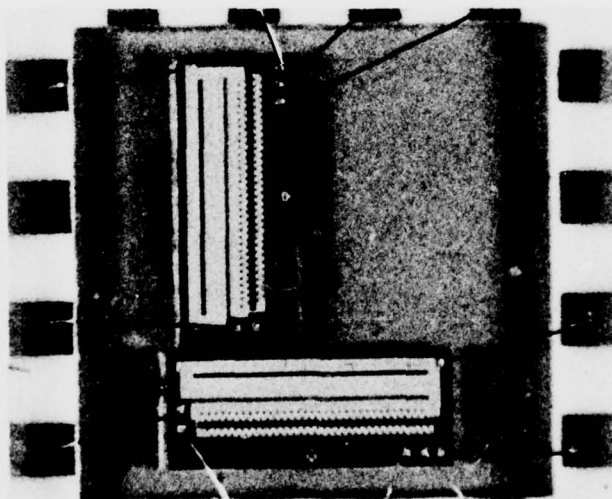


FIG-5

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FIG-4 + 5

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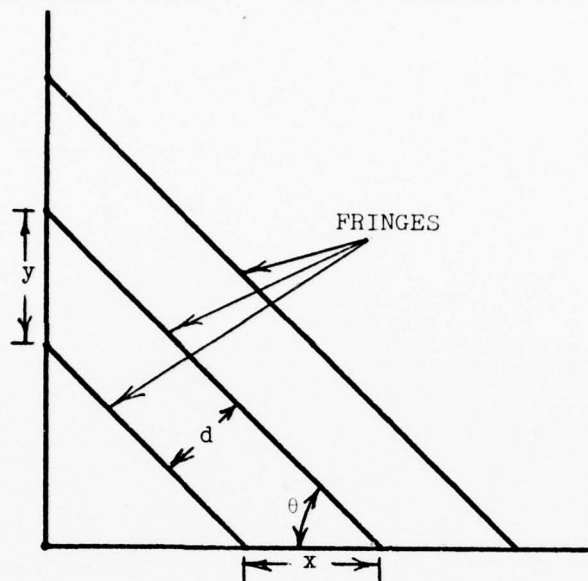


Figure 6. Graphical Description of Angle and Spacing Calculation

SECTION IV

DIGITAL AND ELECTRONIC SETUP

1. COMPUTER MODEL PDP-11-05

The nucleus of the entire specklegram analysis system is a Digital Equipment Corporation Model PDP-11-05 minicomputer with 4000 decimal word storage at 16 bits per word. The computer performs, under program control, all calculations on the incoming data, the stepping sequence of the x-y translation stage, the addressing of the detector, the scanning of the detector, and the retrieval of the data through an A/D converter. Figure 7 is a graphical layout of the processor and its peripheral hookup. A brief sequence of extracting data from a specklegram might be as follows: 1.) Load the plate into its holder and position it to a starting point at the edge of the data array. 2.) Set up the optics for the recorded magnification. 3.) Initialize all peripheral devices. 4.) Enter the x-y stage point differential (stepping resolution). 5.) Step the plate to its first data point. 6.) Address the detector array and perform the detector scan. 7.) A/D the serial data into core memory. 8.) Process the data into fringe spacing and angle. 9.) List the data to the teletype and, 10.) Step to the next data point and repeat the process. At the end of the complete process, the x-y scan parameters can be re-entered and a finer or coarser scan can be performed, based on the previous data run. At this point a more detailed discussion of the procedure for performing Steps 5 and 6 in the above sequence will be discussed.

2. X-Y STEPPING STAGE

The x-y stepping stage (Step 5) assembly consists of a Yosemite 5 inch by 5 inch translation stage, two Slo-Syn stepping motors, two Aerotech Drive Units, and a custom built plate holder mounted to the x-y stage. Stepping of the motors is accomplished by shifting pulses in a serial string to the motors. Each pulse rotates the motors 1.8° (200 pulses - 360°), and the polarity of the pulse determines the direction of motor rotation. The motor driving pulses and their

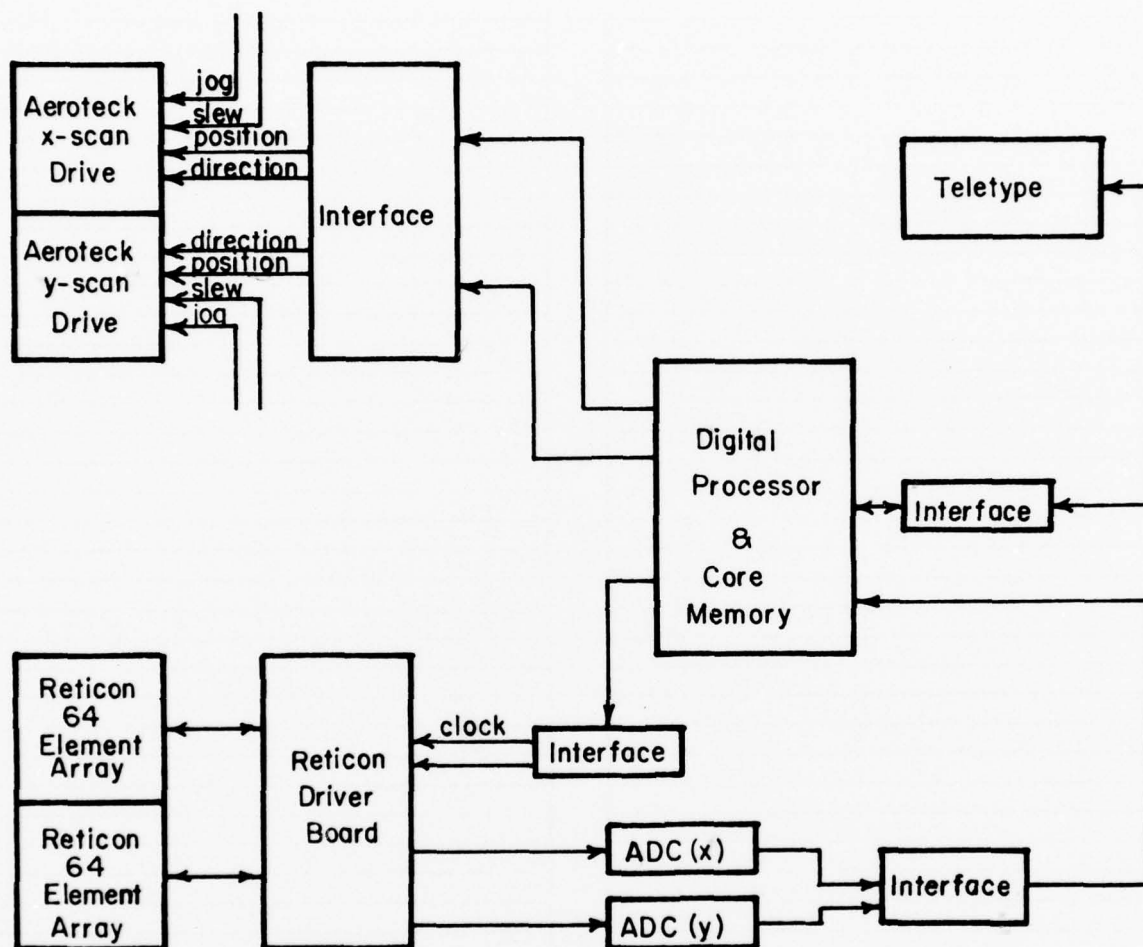
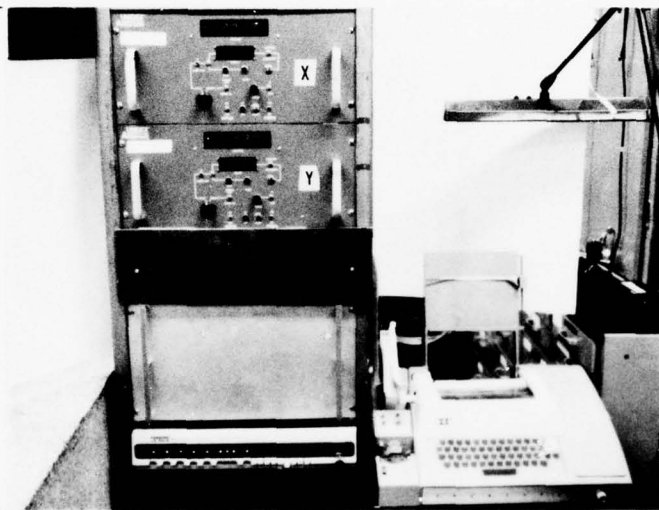


Figure 7. PDP-11 Computer and Peripheral Hookup

polarization are generated by the Aerotech Drive Units and only signals inherent to or input to these drive units will be discussed from this point on. For the case of externally driving the stage, it is required to apply separate 5 volt, 50 μ sec pulses to the Aerotech Drive inputs for rotating the motors, and either a 0 or 5 volt signal to the direction inputs to dictate positive or negative direction of rotation. Each unit has the capability of running internally or externally, and in each case the number of pulses can be monitored by a digital readout on the front panel of the unit. Figure 8 shows the 2 Drive Units in their rack mount. During internal operation, for use in initializing plate position, the motors can be stepped in single pulse mode or in the slow mode; this will repetitively transmit pulses to the motors at a rate preset by a potentiometer on the front panel. Another necessary feature of the internal operation is the ability to reset the digital counter at any time during operation, which will create a zero start reference point. Thus, the drive units can be set to internal operation for initializing the x-y plate position, zeroing the digital meter, and then switching to the external mode for the minicomputer to take control.



Figure 8. Digital and Electronic Hardware



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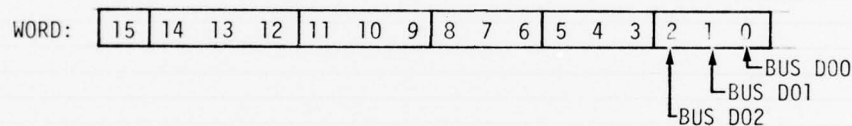
FIG-8

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Since no commercial interface cards were available to drive the Aerotech Units externally, a computer interface was constructed in-house to generate the required driving signals. Figure 9 is a schematic of the interfacing circuitry.

Four signals had to be generated to drive the x-y stage under computer control, two directional signals and two scanning signals. For simplicity, discussion will be limited to only the x portion of the staging, assuming the y portion to be self-explanatory. The x-clock output supplies 50 μ sec, 5 volt pulses to the x-drive unit as required, to drive the x-scanning motor. In order to get a pulse out to the x-clock line through the Figure 9 electrics, a signal has to be applied to lines D1 and E1, simultaneously activating the D303 one shot gate, which, depending on the capacitor value tied to the one-shot, will produce a low voltage 50 μ sec pulse (capacitor = .022 μ f). This output pulse is then amplified to a 5 volt pulse with an operational amplifier tied to a 5 volt, 1 kilohm resistive network. The problem now is to determine how the computer uniquely addresses the lines D1 and E1. D1 is hooked to V2 and an output from this AND gate is achieved by applying a signal on BUS D00, since the other gate input is always set high. The three BUS lines are simply binary outputs defined as follows:



where: the numbers 1-15 represent power of 2,

thus: 1 = BUS D00
 2 = BUS D01
 4 = BUS D02

E1 is hooked to the AND Gate with inputs S2 and N1. The details of these outputs can be referenced in the Peripheral Handbook under the M105

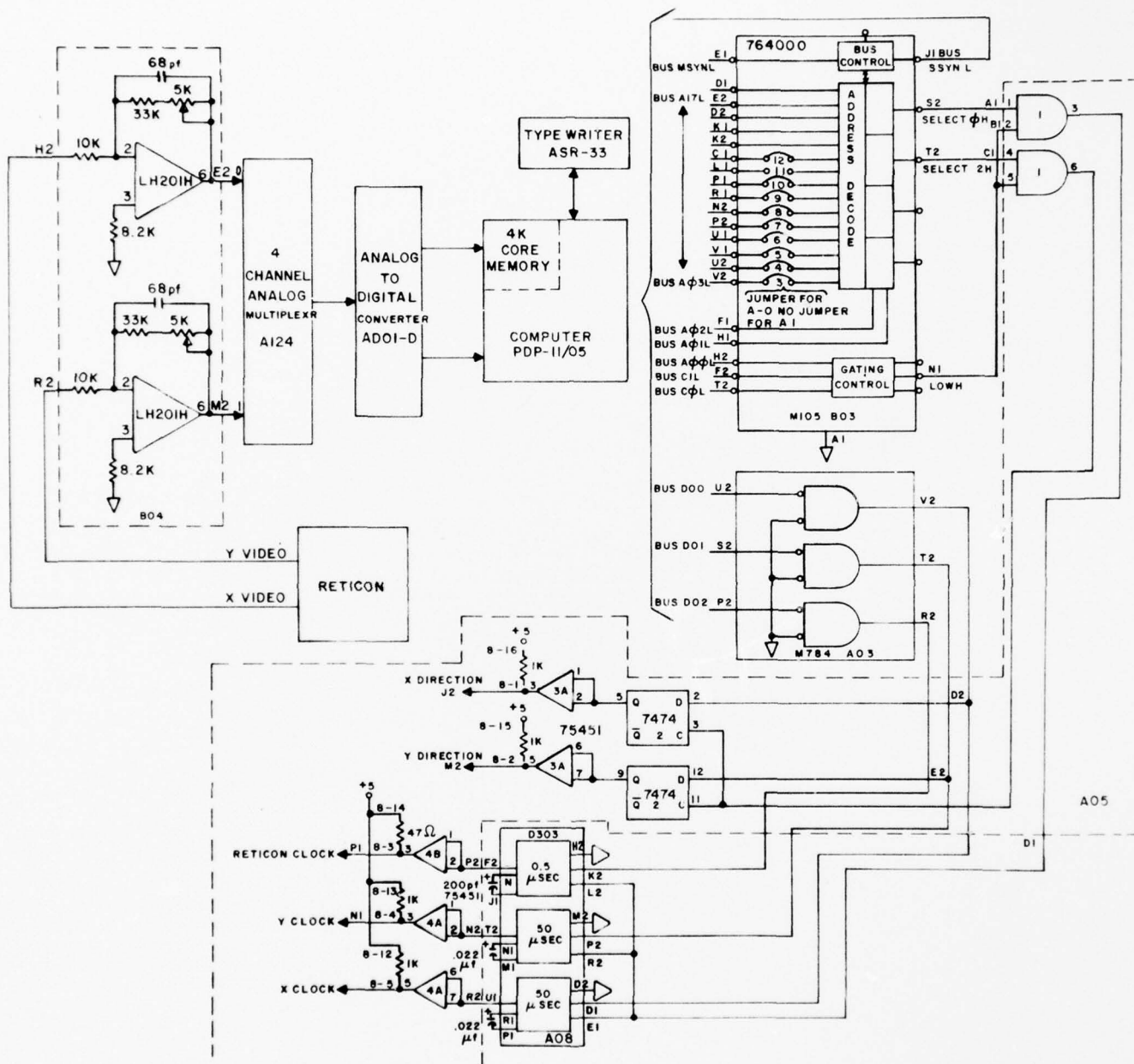


Figure 9. Peripheral Driving Electronics

circuit card chapter. For all practical purposes, in understanding this circuitry, the address to output a signal at point S2 is 164000 and at point T2 is 164002. In total, to get an x-clock output, the number 1 has to be moved to address 164000.

In a similar manner, a table can be constructed to summarize the four x-y stage outputs needed for computer control:

OUTPUT	INPUT	ADDRESS
1. x-clock	001 = 1	164000
2. y-clock	010 = 2	164000
3. x-direction	001 = 1	164002
4. y-direction	010 = 2	164002

3. RETICON DETECTOR ARRAY

Since the specklegram has now been positioned for a data point readout, the detector has to be addressed to read the fringe data. A brief description of the Reticon Array operation would be of assistance at this point. For simplicity, the discussion will be limited to only one of the linear arrays, because the electronic inputs affect both arrays simultaneously.

Each linear array consists of 64 individually addressed detector elements, which are interrogated one at a time by a scanning clock and the charge accumulated by each element is read and cleared upon interrogation. These clock pulses can be generated internally by a separate clocking circuit at a preset rate or can be input to the clocking circuit from an external source at any rate up to 10 MHz, provided the pulses are at least .5 μ sec in duration and 5 volts in amplitude. Whether from an internal or external clock source, the pulses must pass through additional circuitry to be counted for the purpose of generating start and end of scan pulses. The clocking circuit board has 12 binary switches (Figure 10) for setting the time delay (number of pulses delay) desired between readings, thus the maximum delay is $2^{13}-1$ (8191 pulses). At the end of each scan an end



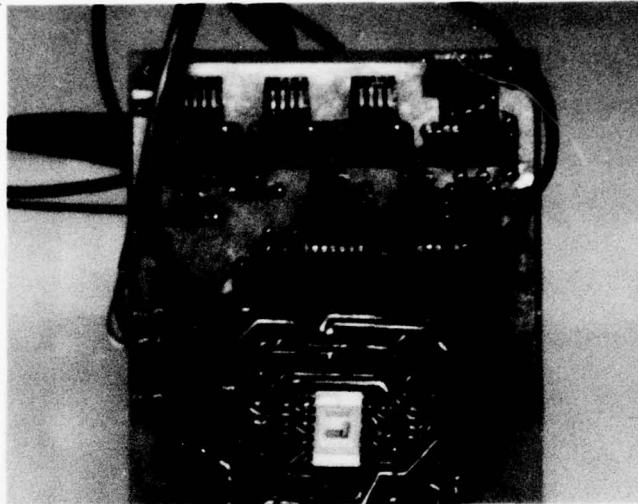
Figure 10. Toggle Switch Configuration

of scan pulse is generated for external triggering and immediately before each scan a trig pulse is generated also for internal triggering. Referring to Figure 11, a typical scan for taking a single data reading is illustrated, with three lines of information. The top line represents the fact that the data is being read to the computer by a negative going pulse, the middle line shows the data itself, and the bottom line shows the end of scan pulses. As can be seen, there are actually two complete scans of the detector elements, before the third scan is read into the computer. The reason for the three scans is that, since the detectors integrate the light incident upon them up until they are interrogated, the first scan most likely will be saturated with ambient light as seen by the center scan at the far left of the figure. The second scan sometimes does not contain all 64 elements of detector information; thus the third scan is the first complete scan containing the data information only. An expanded view of the third scan computer reading, data display, and end of scan pulse is given in Figure 12.

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FIG-10

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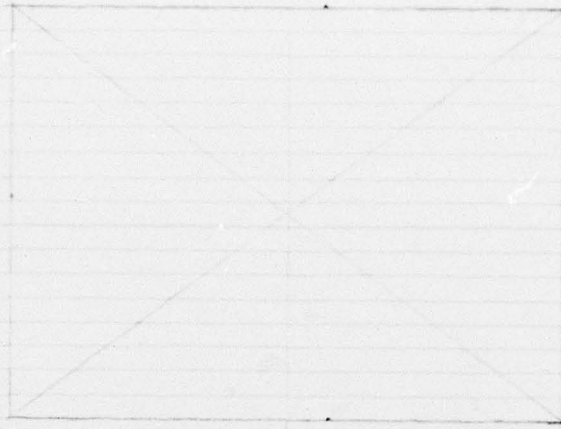


Figure 11. Clock Sequence for Read Initialization

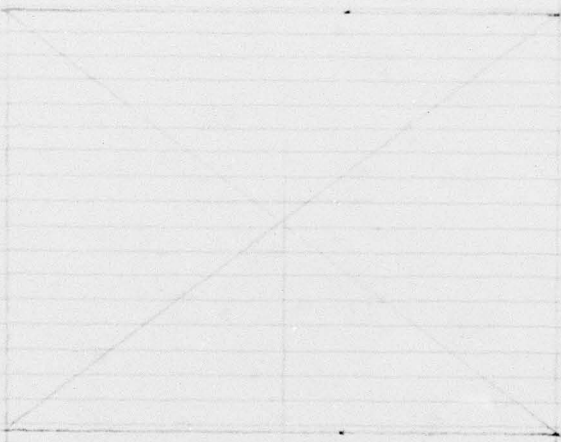


Figure 12. Clocking Sequence for Read Operation

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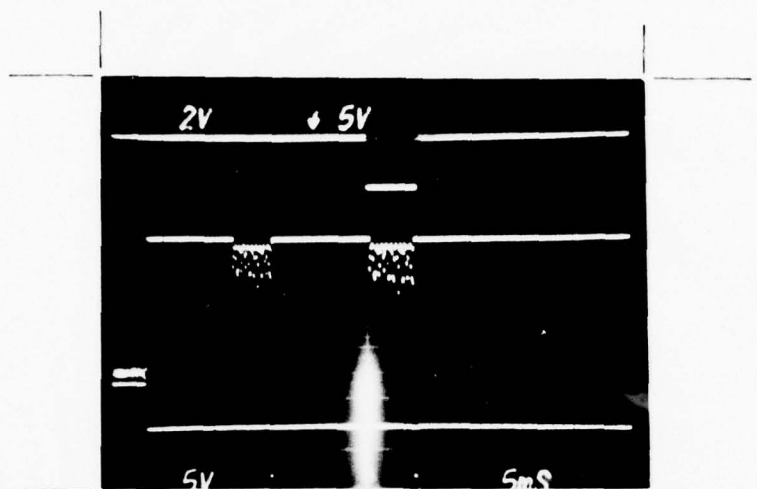


FIG-11

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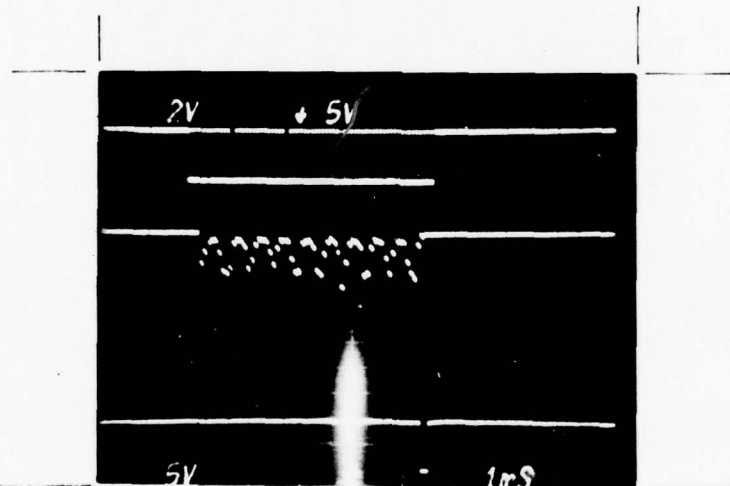


FIG-12

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FIG-11 + 12

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Referring to the schematic of Figure 9, let's now look at the circuitry built to generate the clock pulse and A/D the data to the computer. The same address decoder and input BUS word are used to generate the clock pulses.

OUTPUT	INPUT	ADDRESS
RETICON	100 = 4	164000
CLOCK		

A 200pf capacitor is tied to the the D303 one shot, giving a 5 μ sec pulse output.

Special circuitry had to be constructed to match the Reticon data output to the input of the 4 channel Analog multiplexer (Model A-124). The multiplexer, A/D converter combination requires a 0 to 10 volt input swing to give the full 2^9 levels of digital resolution; thus a variable operational amplifier circuit is used to gain the maximum resolution of the A/D converter by taking the reticon 3 volt signals to the 10 volt maximum. The end-of-scan pulse is input to the 3rd channel of the multiplexer directly and is used to synchronize the software program to the detector and electronic hardware.

Two cash boards had to be attached to the outputs of the data from the reticon to act as a sample and hold circuit to maintain the data from each detector pulse long enough for the A/D converter to read its value. Figure 13 shows two data outputs before and after the cash board circuitry. Notice the short length of time the detector output remains peaked without the Cash Board.

Figure's 14, 15, and 16 are a few examples of 1,2, and 9 fringe outputs respectively. In the lower left hand corner of the figure is an oscilloscope trace of the reticon array output, with its analog to digital conversion data retrieved from computer core, to the immediate right and a graphical plot of the digital data is displayed above the computer printout. Notice how closely the detector output matches the graphical plot of the computer data.

Fig 13

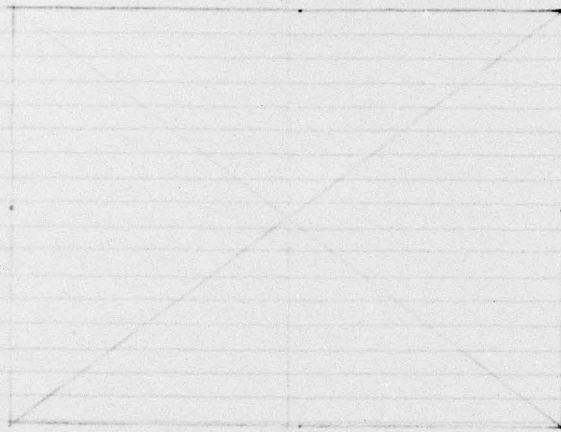
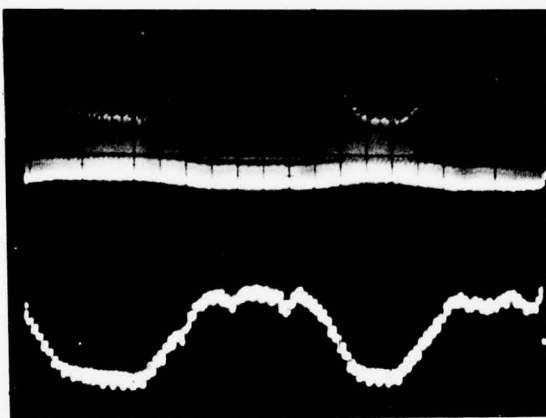


Figure 13. Sample and Hold Illustration

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S/S

AFAL-TR-77-203

FIG-13

PAGE-20

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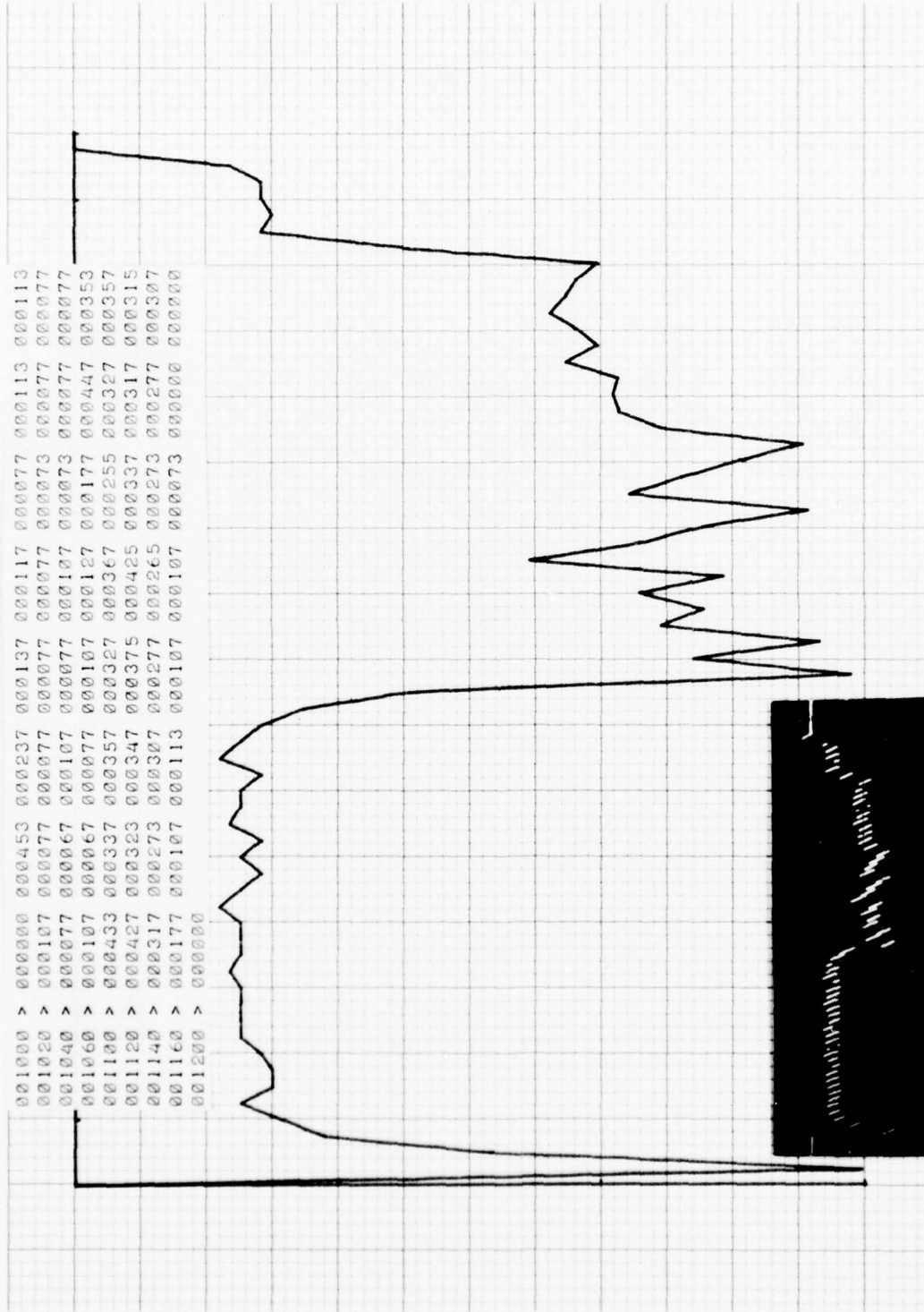


Figure 14. 1Hz Input Fringes With Reticon Plot and A/D Listing

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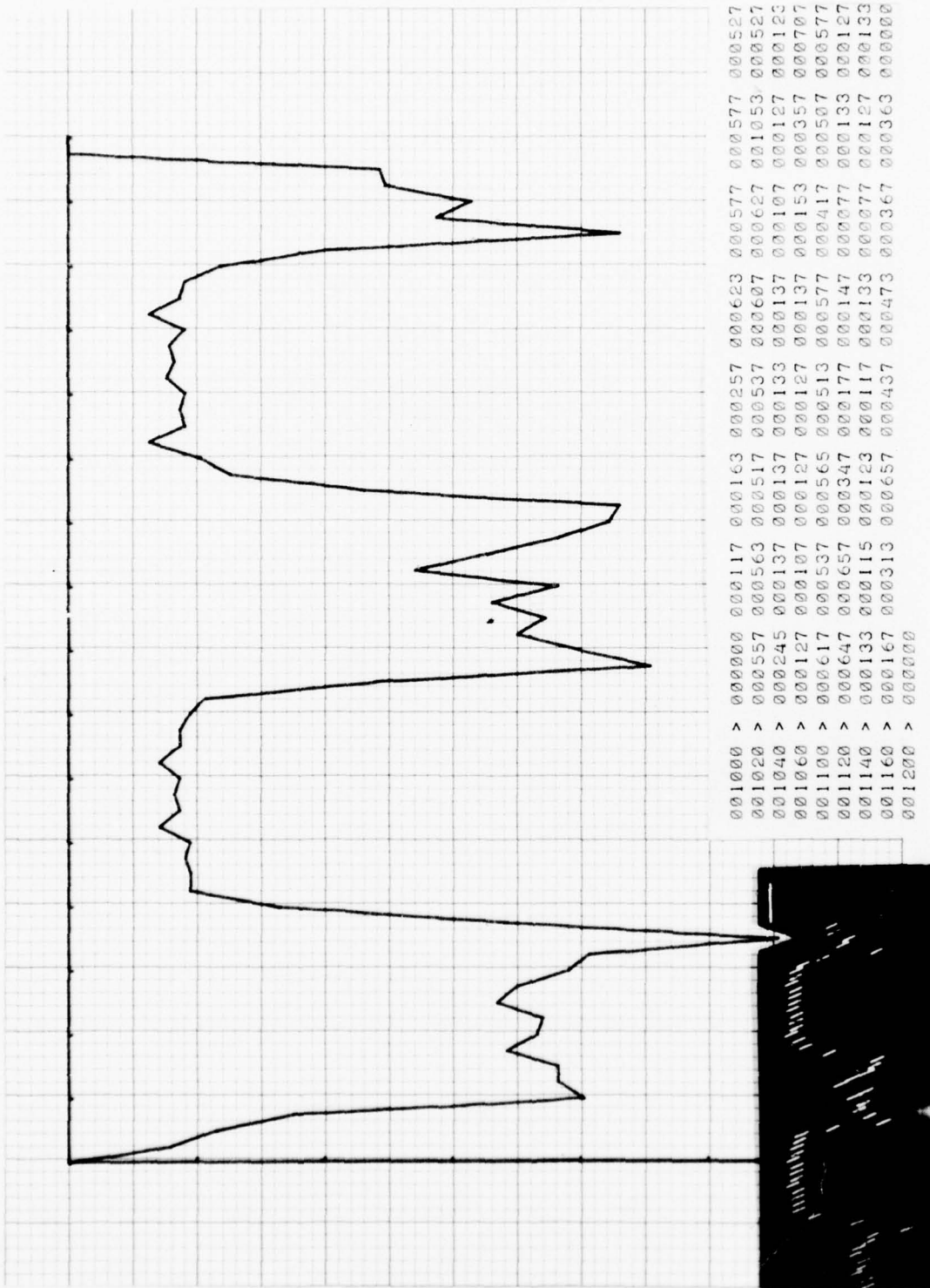


Figure 15. 2Hz Input Fringes With Reticon Plot and A/D Listing

SECTION V

SOFTWARE

1. PDP-11 SOFTWARE FUNCTIONS

The PDP-11-05 family of minicomputers operates on simple 16 bit machine language with 7 registers for program manipulation, 2 of which are a stack pointer (R6) and a program counter (R7). The stack pointer acts as storage pointer for keeping track of subroutine jumps and the program counter keeps track of all addressing within a program, including automatic word or byte sequencing.

The method chosen for writing a program depends on the software compilation routine desired by the user to generate the machine language for computer operation. The highest level language that can be used is Fortran but many hardware options have to be tied to the computer hardware directly, and along with the high cost of the Fortran compiler software, a substantial cost increase is realized. Due to the limited budget available, the simplest of all languages was chosen, and other than creating a substantially more complex programming routine, this simple language proves to be adequate for doing the job. This simple language (assembly language) is comprised of the following programming commands:

1. CLR - clear
2. DEC - decrement
3. INC - increment
4. NEG - negate
5. TST - test
6. COM - complement
7. ASR - arithmetic shift right
8. ASL - arithmetic shift left
9. ADC - add carry
10. SBC - subtract carry
11. ROL - rotate left
12. ROR - rotate right
13. SWAB - swap bytes
14. MOV - move
15. ADD - add
16. SUB - subtract

17. CMP - compare
18. BIS - bit set
19. BIT - bit test
20. BIC - bit clear
21. BR - branch
22. BEQ - branch on equal
23. BNE - branch on not equal
24. BMI - branch on minus
25. BPL - branch on plus
26. BCS - branch on carry set
27. BCC - branch on overflow set
28. BVS - branch on overflow clear
29. BVC - branch on less than
30. BLT - branch on greater than
31. BGE - branch on greater than or equal
32. BLE - branch on less than or equal
33. BGT - branch on greater than
34. BHI - branch on high
35. RTS - return from subroutine
36. JSR - jump to subroutine
37. HALT - halt
38. WAIT - wait for interrupt
39. JMP - jump

The modes available for applying the above commands are listed briefly on the following tables and are described in detail in the PDP-11 Processor Handbook.

MODE	R
------	---

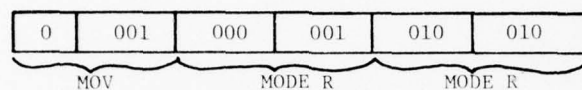
MODE	NAME	SYMBOLIC	DESCRIPTION
Ø	REGISTER	R	R is operand
1.	REGISTER DEFERRED	(R)	R is address
2.	AUTO INCREMENT	(R) +	R is address; $R + 2 \rightarrow R$
3.	AUTO INCREMENT DEFERRED	@ (R) +	R is address of address; $R + 2 \rightarrow R$
4.	AUTO DECREMENT	- (R)	$R - 2 \rightarrow R$; R is address
5.	AUTO DECREMENT DEFERRED	@ - (R)	$R - 2 \rightarrow R$; R is address of address
6.	INDEX	X (R)	$R + X$ is address
7.	INDEX DEFERRED	@ X (R)	$R + X$ is address of address

MODE	7
------	---

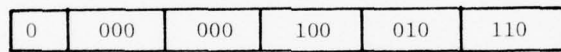
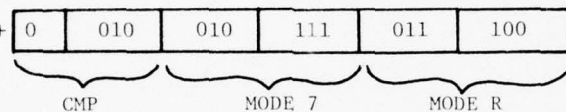
MODE	NAME	SYMBOLIC	DESCRIPTION
2	IMMEDIATE	# n	operand n follows instr
3	ABSOLUTE	@ # A	address A follows instr
6	RELATIVE	A	instr address + 4 + X is address
7	RELATIVE DEFERRED	@ A	instr address + 4 + X is address of address

Three examples using the commands and modes listed above are given as follows.

MOV R1, (R2) +

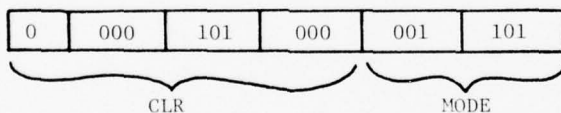


CMP # 426, @ (R4) +



0 0 0 4 2 6

CLR (R5)



2. CONTROL PROGRAM SOFTWARE DESCRIPTION

Due to the limited commands and the lack of arithmetic functions, the software required to control the complete analysis system is quite complex and lengthy contrary to what might be expected when using a higher level language. The program can be outlined into 21 different sections or subroutines as follows.

1. PROGRAM START AND PARAMETER LOADING - START
2. ASC II AND DECIMAL TO OCTAL CONVERSION - ASC II
3. CONTROL - MANIP
4. FAST FOURIER TRANSFORM - FIT
5. DETECTOR READ - READ
6. DISPLACEMENT & ANGLE LIST - PRINT
7. ANGLE CALCULATION - ANGLE
8. AMPLITUDE CALCULATION - AMP
9. TELETYPE OUTPUT - TTYOUT
10. OPERATION SELECTOR - OPER
11. TELETYPE INPUT - INPUT
12. DISPLACEMENT CALCULATION - DISP
13. FRINGE FREQ DETERMINER - FREQ
14. OCTAL TO DECIMAL CONVERSION - OTD
15. X-Y STAGE CONTROL - STAGE
16. PRINT POSITION - POSITN
17. DATA BUFFERS - RRØ - STEPLY
18. PRINT BUFFERS - ASKAV - QUES
19. TRIG TABLE FOR ANGLE - TANBUF - SINBUF
20. TRIG TABLE FOR FFT - COS - SIN
21. SYMBOL TABLE - A - ZEROX

Each subprogram can be described briefly in the order that it appears in the overall program as follows:

1. TITLE merely sets a title heading for the program that appears at the top of each page.

5. ENABLE AMA sets the assembler to define the machine language in the Absolute Memory Addressing mode.

8 - 15 These lines define the labels assigned to the bottom 7 words of core in computer memory with register numbers, stack pointer, and program counter.

16 - 19 Lines define the labels assigned to the listed core locations 177560-177566 which address the input and output from the teletype terminal. KBS and TPS are merely status words and KBB and TPB are input and output buffers.

27. 500 is the starting address of the program.

28. START: This is the first line of the main program which assigns a stack pointer address.

30 - 31 Prints "No. of Data Averages" by addressing the TTYOUT Subroutine.

32 - 37 Loads ASC II value of No. of Averages to the "MEAN" buffer via the INPUT subroutine and then converts the ASC II values to an octal value and stores it in the TIMES buffer.

39 - 42 Clears all buffers from X LIMIT to STEP-X in the data buffer subroutine called RRØ.

43 - 75 Prints enter, and convert to octal: "X-Tot Scan Distance," "Y-Tot Scan Distance," "X-Increment," and "Y-Increment," similar to the method described in lines 32 - 37.

68. Sets the direction of the X and Y scan to be positive. Referring to Figure 9, move a 4 to 164002 which moves zeros to 164002 through Bus D00 and D01, making the output to the direction lines 0 volts or "low" produce a positive direction.

76 - 77 Prints the header title as shown in the data section of this report.

78 - 79 Jumps to the subroutine "STAGE," which initiates the X-Y stepping stage.

80 - 81 Prints "X-Y SCAN COMPLETED."

83. Halts.

86 - 90 ASC II: Subtracts 60_8 from each ASC II entry; thus the member 61_8 (ASC II for 1) - $60_8 = 1_8$ and 71_8 (ASC II for 9) - $60_8 = 11_8$, which continues until a carriage return is received (#15).

92 - 94 Loads Least Significant Digit, which is already in octal format.

98 - 104 Converts 2nd digit to octal format as follows:
Add 12_8 (10_{10}) to a dummy register for each unit value in the 2nd digit and then loads the final value to R3, which is the finish of the ASC II routine, and is the final octal value of the complete list of digits.

105 - 132 Converts the 3rd, 4th, and 5th digit in the same manner as in steps 95 - 104.

133 - 135 Stores final answer in OBUF.

138 - 142 Clears working registers and buffers from RRO to KEEP (lines 892 - 911).

143 - 140 Clears FBUFAV and FFTBUF.

147 - 153 Self explanatory.

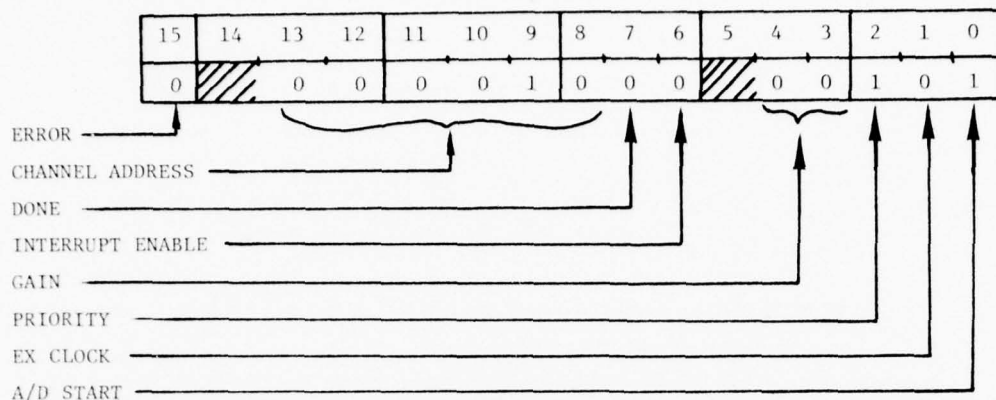
154 - 158 If the frequency is below 4 fringes then prints "LOW;" if not, then prints Go To a Frequency.

159 - 162 Changes Octal Frequency Count to Decimal Value and converts to ASC II Code; then prints value in Base 10 to Teletype Output Printer.

163 - 175 The first time through MANIP performed complete analysis on X direction of Detector data, and now the Y-direction data is analyzed through MANIP and printed out to TTYOUT.

178 - 462 FFT: Due to the complexity of the Fast Fourier Transform Routine details of its operation can be obtained from Mr. Lane of AFAL/DHO, and will not be covered in this report.

471. READ: Moves a clock pulse from the Electronics Unit schematically illustrated in Figure 9 to the clock input of the Reticon Array.



472. Moves the number 1005_8 to the control and status register (links the A/D converter to the software) which addresses channel 2 of the A/D converter, sets the priority level to 1 and starts the A/D operation.

473. Loads the CSR (Control and Status Register) to R0.

474 - 475 Checks for the Done Bit of CSR (Bit 7), and if not sets return to DONE 1, otherwise must go to next line and load data.

476 - 478 Moves the data from channel 2, through data Register 176772, to register R1. Channel two is hooked to the detector end of scan (EOS) line which emits a pulse when a complete scan of the 64 detector elements is finished. After the data load, the program checks to see if the end of scan pulse has appeared. If not, branches to CLOCK 1.

479 - 482 Allows for 2 EOS pulses before continuing to the next program section.

483 - 487 Continues clocking the detector through the dead time between scans that are preprogrammed through the toggle switches on the clocking circuit board. The switches are set to

$$0000 \quad 1111 \quad 0011 = 227_{10}$$

Thus, it works out that 202, as programmed in the software, provides the proper delay to allow a data read at the correct time.

488 - 491 Is a software delay that allows a large enough time between clock pulses, for the pulse generator of Figure 9, to operate properly. If, for instance, the MOV # 4, @ # 164000 operation were performed in a small program loop, the pulses generated from the address decoder, arrive at too high a rate for the one-shot delay, thus exiting at the clock pulse output as a voltage level, not a pulse.

492 - 494 Decides whether to read the X detectors or the Y detectors.

495 - 500 The entire clocking routine previous to these steps were initialization procedures aimed at setting up the A/D converter to read data from the detector array at a time when meaningful data was present. These few lines read this unambiguous data and load it into core memory. (R4) is the storage medium where R4 points to either FFTBUF or FBUFAV.

505 - 512 If averaging of the data is desired, which is a buffer that designates a data load to either FFTBUF, or FBUFAV.

513 - 525 Repeats the data read operation for the Y-axis with the same logic as in steps 492-509.

526 - 540 Averages the data and loads the averaged data to the FFTBUF buffer. Since the averaging method probably does not appear obvious, a brief description follows: 523 - 525 TIMES contains the number of desired averages with TRACK incrementing with each average performed (TRACK = TIMES means done). 526 - 527 The data is loaded to FFTBUF from the first data read; 528 - 534 after first two data reads, each data buffer (FFTBUF: FBUFAV) is divided by 2 (ASR) added together and loaded to FFTBUF. 535 - 537 Prepares to load new data to FBUFAV for another average.

543 - 549 Allows for reduction of redundancy between first and second half of the detector active elements by loading the data stored for the first half of the detector into the storage location delegated for the second half.

555. PRINTS.

556 - 562 Clears the XDIST0 and YDIST0 buffers; then calculates the X-spacing from the X-frequency as follows: $(f/\text{No. of detectors} = \text{spacing})$ where $f = \text{ROBUF}$, No. of detectors = $64_{10} = 100_8$.

563 - 567 Same as above for Y-spacing.

568 - 576 Goes to Angle calculation subroutine; then returns and prints answer. Goes to Displacement subroutine; then returns and prints answer.

581. ANGLE.

582 - 593 Loads X and Y spacings; multiplies the Y spacing by 100₈ to obtain a whole-number output from the division of Y by X. The angle is calculated by:

$$\theta = \tan Y/X$$

594 - 599 Takes the value Y/X (stored in R0) and scans it through the tangent table (TANBUF), listed in one-degree increments, until the two values compare; then stores the comparison address to RATIO.

600 - 607 Clears DBUF then Jumps to Subroutine OTD and loads to DBUF.

612. AMP.

613 - 620 Loads start address for Real Part of FFT (FFTBUF) and imaginary Part of FFT (FFTBUF + 200). Checks to see if data point of real and imaginary are negative, if so make positive.

621 - 628 Squares the real data point amplitude.

629 - 641 Squares the imaginary data point amp.

637 - 641 Adds real and imaginary data points and moves to original real data point storage location and checks to see if all data points have been squared; if not, increment the FFTBUF addressed for real and imaginary and repeats the complete process starting at line 615.

651. TTYOUT.

651 - 656 Tests the Teleprinter Status; if read, moves data to Teleprinter Buffer and prints. Checks if finished printing by a 0 data point appearing.

661. OPER.

661 - 678 Checks if a given letter (S, X, Y, or D) was input from the Teletype and, if so, load R5 accordingly.

683. INPUT.

683 - 687 Checks the Keyboard Status and, if ready, moves the ASC II code of the desired key to R4; then clears the part bit (Bit 7) and moves the answer to address of (R0).

696 - 702 Prints correct character; checks if input is completed (#15 - Carriage Return) and moves a line feed to the printer (#12).

704. DISP.

704 - 707 Moves Sin Buffer address to R1 and adds RATIO to it. Ratio contains the address representation of the angle calculated in the ANGLE subroutine. Since the Displacement is calculated by

$$d = X \sin \theta$$

and the sin of θ can be calculated from a table similar to TANBUF, called SINBUF, which is also set up in one-degree increments; d is easily obtained by multiplying X by the value obtained from the SINBUF table.

708 - 723 Multiplies X DISTO by sin θ and divides the answer by 100_8 since SINBUF value is premultiplied by 100_8 ; then the answer is changed to decimal and control is returned to PRINT.

727. FREQ.

729 - 731 Checks for a high amplitude D.C. component in the FFT Data; if lower than 156, sets H1DC.

732. FFTBUF + 140 represents a fifteen Hertz frequency bin and, for determining the frequency, it is assumed that no frequency will be higher than 15 Hz or 15 fringes.

733 - 738 Checks for highest amplitude frequency bin by comparing the amplitude of the presently addressed bin to the maximum amplitude of all the previously searched bins; if larger goes to HOLD. If it is smaller, increments the next bin and either returns to search at SRCH or moves to QUIT if all bins have been searched.

739 - 747 For H1DC, checks data with #10 amplitude; if below GTO QUIT - 6.

748 - 750 If frequency was valid, loads address to R2 and the amplitude to R3, the increment between data point scans.

753 - 757 If no frequency was stored ($R3 = 0$), then moves 1 to NONE.

758 - 765 Looks at amplitudes on both sides of the highest amplitude frequency bin (R3) and determines if the actual frequency is slightly higher or lower than R3 by loading 1 to R5, if above; and loading 0 to R5, if below.

766 - 769 Since $FFTBUF + 200$ is 0 frequency and each bin in the $FFTBUF$ is one cycle, then subtracting R2 from $FFTBUF + 200$ and dividing the answer by two, results in the final frequency in Hertz.

770 - 777 Loads the frequency to OBUF and a + or - to $OBUF + 2$. Returns control MANIP.

786. OTD.

786 - 822 Changes data in OBUF to a base 10 equivalent; then converts to ASC II code for printout.

827. STAGE.

832 - 840 MOV #1, @ # 164000 sends a X-clock pulse to the X-Y stage driver. Unit keeps track of the number of pulses transmitted for each scan between data points, whereas LINE keeps track of the total number of pulses transmitted to the total X-scan for one line. DELAY simply stores a programmed delay to allow the pulses to zero before another signal appears. Unit is compared to STEP X which contains the data determining the increment between data point scans.

845 - 848 Checks to see if the end of line distance is reached; if so, Branch to ZEROX.

865 - 873 Changes the sign of X and sends pulses to drive the X unit until the X position is 0 or its original position. A long delay is required (40000) before further execution of scanning to allow for experimental stabilizing. At this point the X sign is changed again and a Y scan is performed.

883. POSITN.

883 - 886 Clears the Decimal Buffer (DBUF).

887 - 890 Loads the X-position in octal and converts to decimal for terminal printout.

891 - 896 Same as above for Y-position.

897 - 900 Reloads the data point scan separation and returns to STAGE subroutine.

The last two pages of the program are a table showing the numerical address assigned to all Labels in the program.

The description of the software for operating the overall System, has been explained only in brief for the purpose of this report and a more detailed discussion can be planned upon request by the Flight Dynamics Laboratory.

SECTION VI

DATA

In this section of the report we will discuss the individual data shown in Figure 17 through 30 and the significance of the overall data collection as presented in the Results Section. A complete data collection operation had not been performed at the writing of this report, but shortly thereafter, it was anticipated that a complete set of data would become available for listing to the Flight Dynamics Laboratory.

The first method pursued for analyzing specklegram data was to look for amplitude peaks or nulls in the detector scanned data signals and average the distance between each peak or null by counting the number of detectors lying between them.

For initial experimental trials a set of fringe negatives were constructed photographically to input to the optical systems as a sample of high contrast fringes for setting up the computer software. Some data from these initial runs is shown in Figures 17, 18, 19, and 20. Frequencies of 5 Hz, 6 Hz, 7 Hz, 8 Hz, 9 Hz, 10 Hz, 20 Hz, 30 Hz, and 40 Hz were the photographic inputs. As can be seen, the system operated nearly flawlessly for these types of fringe inputs. At this point some real fringe data was input to the optical system and a couple of the best data runs are shown in Figures 21 and 22. Notice the variance in what appears to be peaks or nulls in the digital data printout. The data for most cases was less impressive than that shown, thus a new method for counting the fringe data had to be established.

Coincidental with our search for a new method of analysis, an electronics equipment oriented company made available an FFT (Fast Fourier Transform) operator for demonstration. This turned out to be the opportunity we needed to see if an FFT program would solve some of the problems we had encountered during peak detection. A typical specklegram data was projected onto a Reticon Array that we supplied and input to the FFT hardware they supplied.

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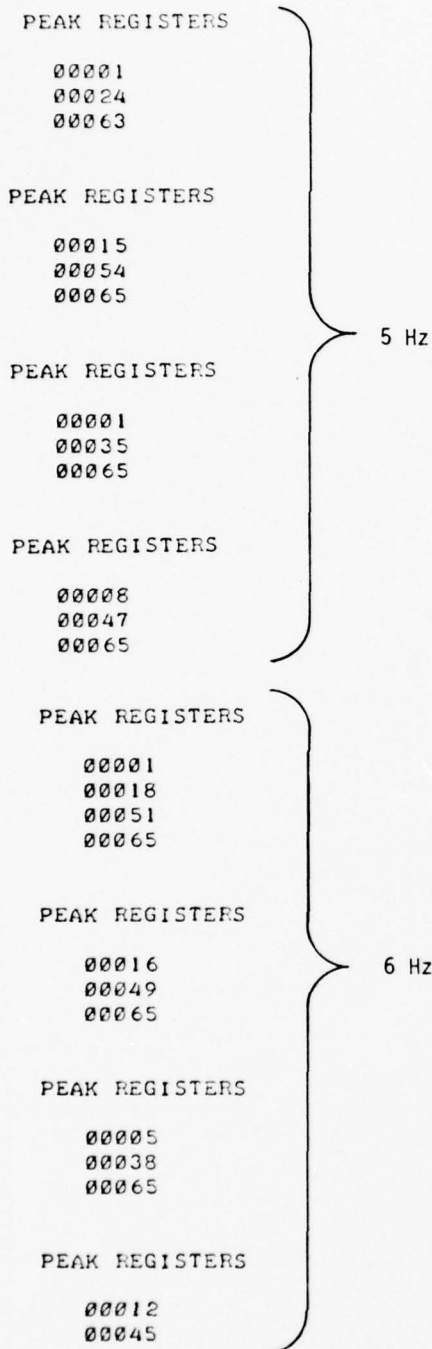


Figure 17. Data Runs With High Contrast, Ideal Fringe Pattern

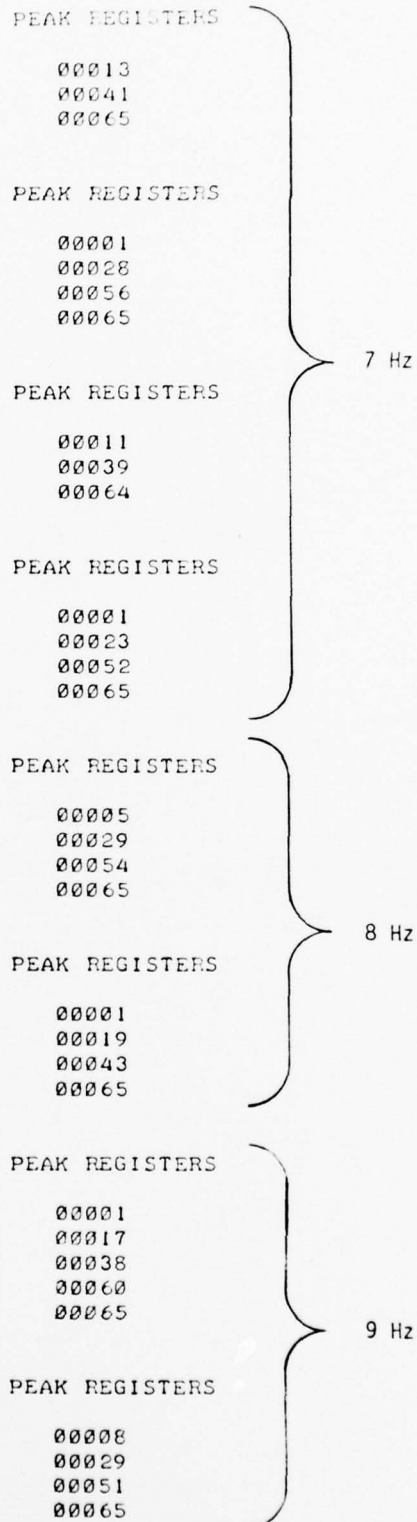


Figure 18. Data Runs With High Contrast, Ideal Fringe Pattern

PEAK REGISTERS

00008
00027
00047
00064

10 Hz

PEAK REGISTERS

00001
00016
00035
00055
00065

PEAK REGISTERS

00003
00013
00023
00032
00042
00052
00062
00065

20 Hz

PEAK REGISTERS

00003
00013
00022
00032
00042
00052
00062
00065

PEAK REGISTERS

00003
00009
00016
00022
00029
00036
00042
00049
00055
00062
00065

30 Hz

PEAK REGISTERS

00003
00009
00016
00022
00029
00035
00042

PEAK REGISTERS

00004
00009
00013
00018
00023
00028
00033
00038
00043
00048
00053
00058
00062
00065

40 Hz

PEAK REGISTERS

00003
00008
00013
00018
00023
00028
00032
00037
00042
00047
00052
00057
00062
00065

Figure 20. Data Runs With High Contrast, Ideal Fringe Pattern

Figure 19. Data Runs With High Contrast, Ideal Fringe Pattern

PEAK REGISTERS

00007
00022
00040
00056
00069

001554 > 000000 000000 000000 000000 000000 000107 000137 000147
001574 > 000237 000427 000757 000477 000577 000377 000457 000307
001614 > 000157 000107 000127 000117 000107 000077 000117 000123
001634 > 000157 000167 000427 000657 000763 000573 000553 000577
001654 > 000673 000323 000225 000153 000133 000107 000117 000113
001674 > 000115 000077 000157 000227 000553 000773 000527 000475
001714 > 000667 000417 000247 000147 000137 000077 000117 000117
001734 > 000117 000077 000133 000213 000477 000777 000657 000563
001754 > 000545 000337 000327 000000 000015 000012 000015

001772 > 000007 000026 000050 000070 000105 000012 000015 000000
002012 > 000000 000000 000000 000000 000000 000000 000000 000000
002032 > 000000 000000 000000 000000 000000 000000 000000 000000
002052 > 000000 000000 000000 000000 000000 000000 000000 000000
002072 > 001657

002074 > 000107 000137 000147 000157 000107 000127 000117 000107
002114 > 000077 000117 000123 000157 000137 000153 000133 000107
002134 > 000117 000113 000115 000077 000157 000147 000137 000077
002154 > 000117 000117 000117 000077 000133 000000 000015 000000
002174 > 000000 000000 000000 000000 000000 000000 000000 000000
002214 > 000000 000000 000000 000000 000000 000000 000000 000000
002234 > 000000 000000 000000 000000 000000 000000 000000 000000
002254 > 000000 000000 000000 000000 000000 000000 000000 000000
002274 > 001566

002276 > 001570 001572 001574 001616 001620 001622 001624 001626
002316 > 001630 001632 001634 001636 001640 001664 001666 001670
002336 > 001672 001674 001676 001700 001702 001724 001726 001730
002356 > 001732 001734 001736 001740 001742 001764 001766 000012
002376 > 000000 000000 000000 000000 000000 000000 000000 000000
002416 > 000000 000000 000000 000000 000000 000000 000000 000000
002436 > 000000 000000 000000 000000 000000 000000 000000 000000
002456 > 000000 000000 000000 000000 000000 000000 000000 000000
002476 > 042520

Figure 21. Data Runs With Real Specklegram Data

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PEAK REGISTERS

```

00009
00021
00034
00047
00061
00069

001554 > 000000 000000 000000 000000 000000 000137 000137 000127
001574 > 000117 000077 000127 000213 000477 000467 000377 000357
001614 > 000417 000137 000127 000133 000117 000077 000127 000127
001634 > 000247 000577 000737 000615 001033 000477 000227 000147
001654 > 000153 000077 000127 000127 000217 000457 000757 000707
001674 > 000653 001113 000473 000177 000157 000077 000133 000117
001714 > 000137 000127 000377 000647 000537 000427 000633 000377
001734 > 000217 000123 000157 000127 000117 000107 000177 000377
001754 > 000647 000347 000253 000000 000015 000012 000015

001772 > 000011 000025 000042 000057 000075 000105 000012 000015
002012 > 000000 000000 000000 000000 000000 000000 000000 000000
002032 > 000000 000000 000000 000000 000000 000000 000000 000000
002052 > 000000 000000 000000 000000 000000 000000 000000 000000
002072 > 001657

002074 > 000137 000137 000127 000117 000077 000127 000137 000127
002114 > 000133 000117 000077 000127 000127 000147 000153 000077
002134 > 000127 000127 000177 000157 000077 000133 000117 000137
002154 > 000127 000123 000157 000127 000117 000107 000177 000000
002174 > 000015 000000 000000 000000 000000 000000 000000 000000
002214 > 000000 000000 000000 000000 000000 000000 000000 000000
002234 > 000000 000000 000000 000000 000000 000000 000000 000000
002254 > 000000 000000 000000 000000 000000 000000 000000 000000
002274 > 001566

002276 > 001570 001572 001574 001576 001600 001602 001620 001622
002316 > 001624 001626 001630 001632 001634 001654 001656 001660
002336 > 001662 001664 001704 001706 001710 001712 001714 001716
002356 > 001720 001740 001742 001744 001746 001750 001752 001764
002376 > 001766 000012 000000 000000 000000 000000 000000 000000
002416 > 000000 000000 000000 000000 000000 000000 000000 000000
002436 > 000000 000000 000000 000000 000000 000000 000000 000000
002456 > 000000 000000 000000 000000 000000 000000 000000 000000
002476 > 042520

```

Figure 22. Data Runs With Real Specklegram Data

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Figure 23 is a four plot sequenced illustration of the result of this mock setup. The first plot shows the specklegram data after and before averaging 512 times (top and bottom respectively). The second plot shows the first FFT with a strong peak to the far left and a secondary peak to its immediate right. The first peak turned out to be the reticon clock frequency and the second peak the actual data frequency. The third plot shows the clock frequency filtered out, thus rendering the strongest frequency peak to be 4.2 KHz instead of the 200 Hz Reticon clock frequency. Plot four shows the inverse transform of the FFT data giving back a signal with the same frequency as plot number 1. Thus it was concluded that the FFT approach would become the solution to the problem.

After an extensive amount of programming was performed to implement an FFT software routine, the photographic fringes were introduced into the system. Figures 24, 25, 26, 27, and 28 show a data run with different frequencies introduced into the x and y detectors of the Reticon Array. Notice please, that each frequency calculated is as nearly right as can be interpreted from the Reticon detector plot shown on the scope traces. The pluses and minuses listed before each frequency indicated whether the frequency displayed is slightly higher or lower than the frequency printed.

The computer listing of Figure 29 is a typical teletype printout obtained during a data run with the software advanced as far as it is today. The first question asks if the user wants a list of the FFT data. The second question asks how many times he wants the fringe data input and averaged before performing the FFT. "OUTPUT" asks if an x or a y detector scan is desired. The next few questions set up the scanning parameters for the x-y scanning stage, and are self-explanatory. At this point the computer takes over and prints out the x and y position of the data plate in the x-y translation stage, the calculated value for the frequency of the fringes, and a "LIST," which is merely a listing of the Fourier Transform of the averaged data, so as to determine if the calculated frequency agrees with the Transform data.

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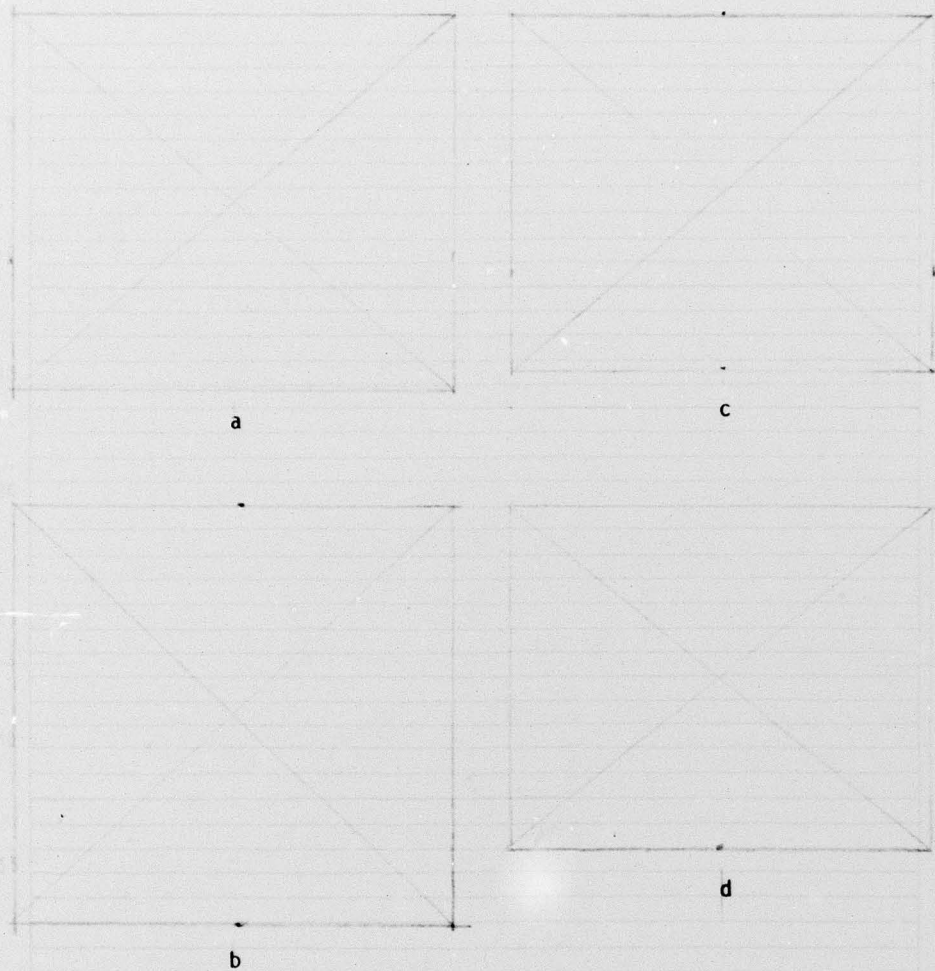


Figure 23. Sample Data Analyzed With Hardware FFT

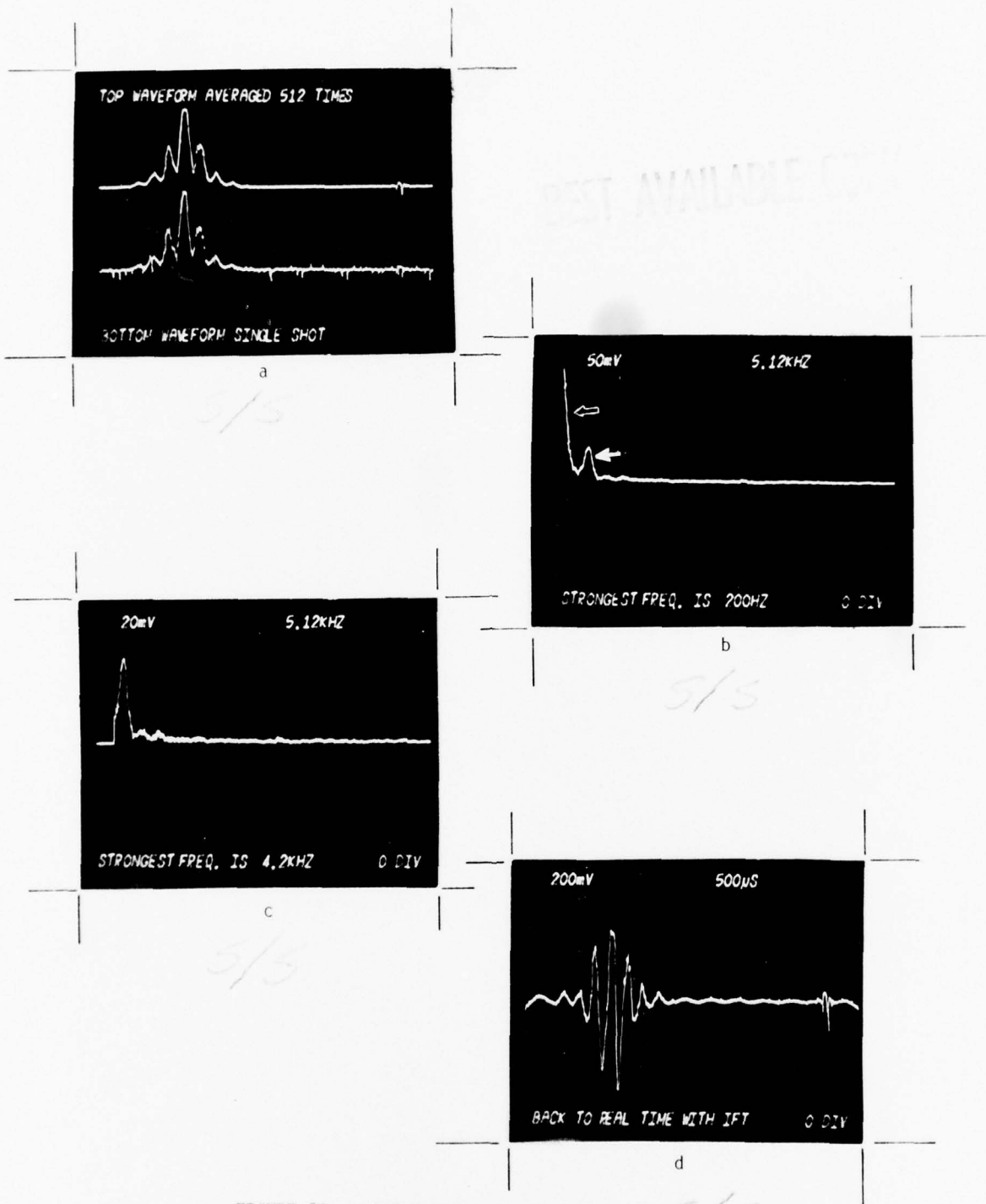


FIGURE 23. SAMPLE DATA ANALYZED WITH
HARDWARE FFT

HFAL-TR-77-203
FIG-23, a, b, c + d
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OUTPUT ? X
FREQUENCY= -00010

OUTPUT ? Y
FREQUENCY= +00003

+

OUTPUT ?



Figure 24. Data With Software FFT

OUTPUT ? X

FREQUENCY= +00005

+

OUTPUT ? Y

FREQUENCY= +00008

+

OUTPUT ?

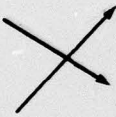


Figure 25. Data With Software FFT

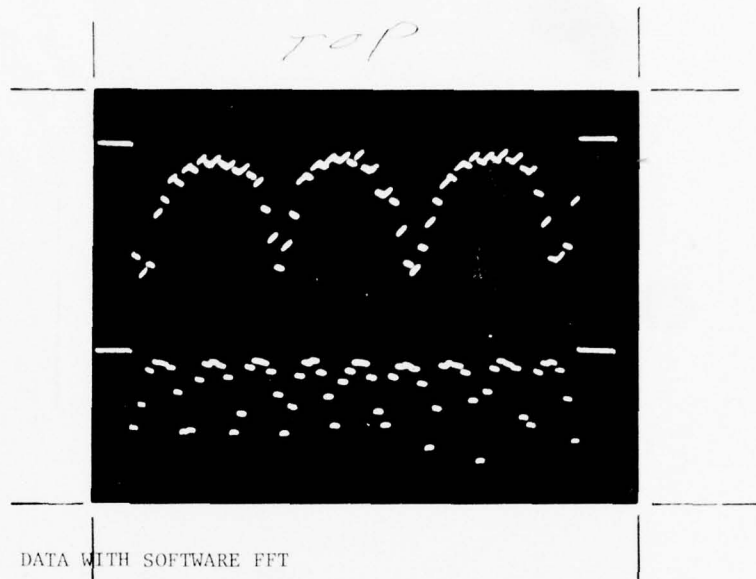


FIGURE 24. DATA WITH SOFTWARE FFT

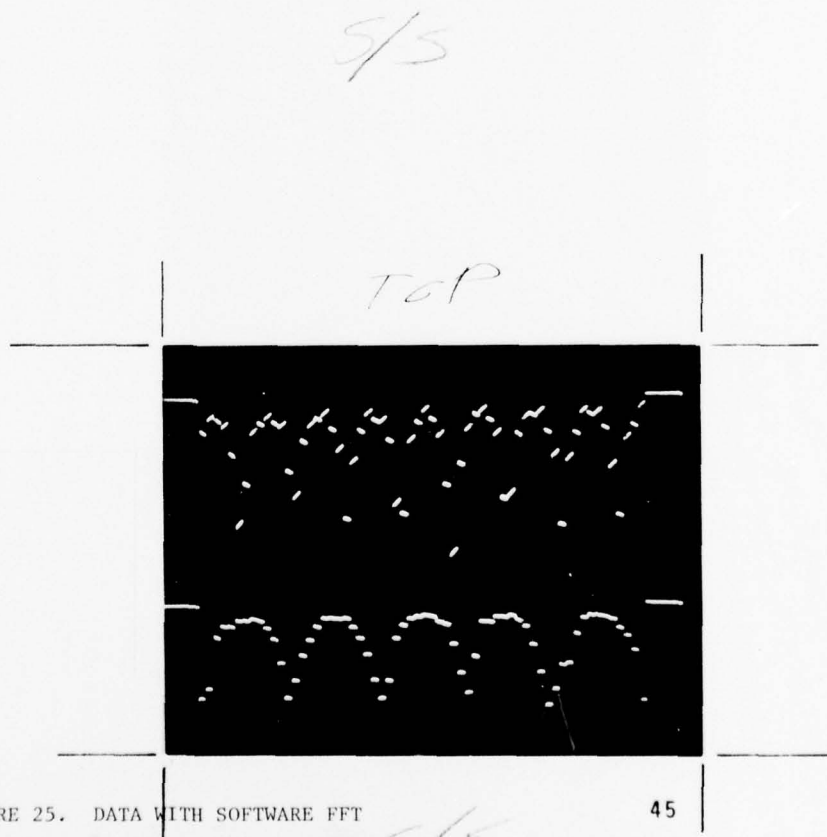


FIGURE 25. DATA WITH SOFTWARE FFT

S/S

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FIG-24+25

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OUTPUT ? X
FREQUENCY= +00006
+

OUTPUT ? YY
FREQUENCY= -00008
-

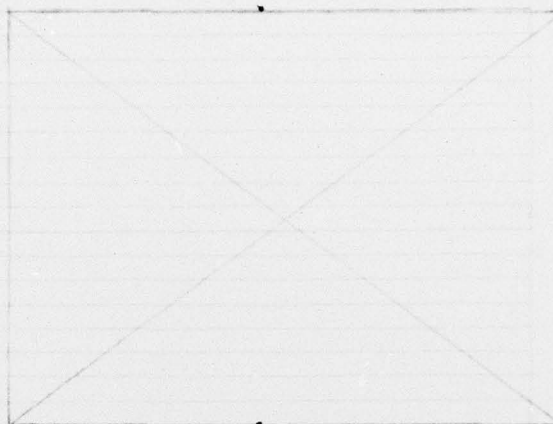


Figure 26. Data With Software FFT

OUTPUT ? X
FREQUENCY= +00008
+

OUTPUT ? Y
FREQUENCY= -00006
-

OUTPUT ?

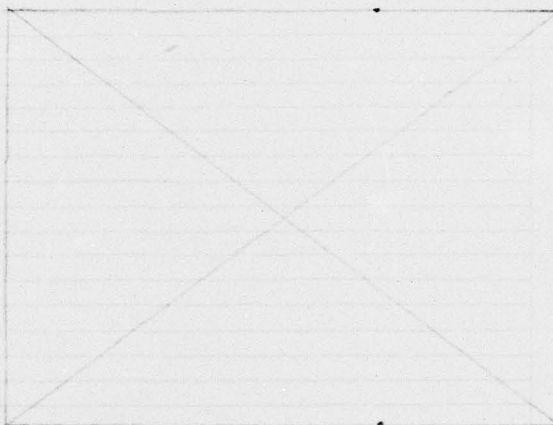


Figure 27. Data With Software FFT

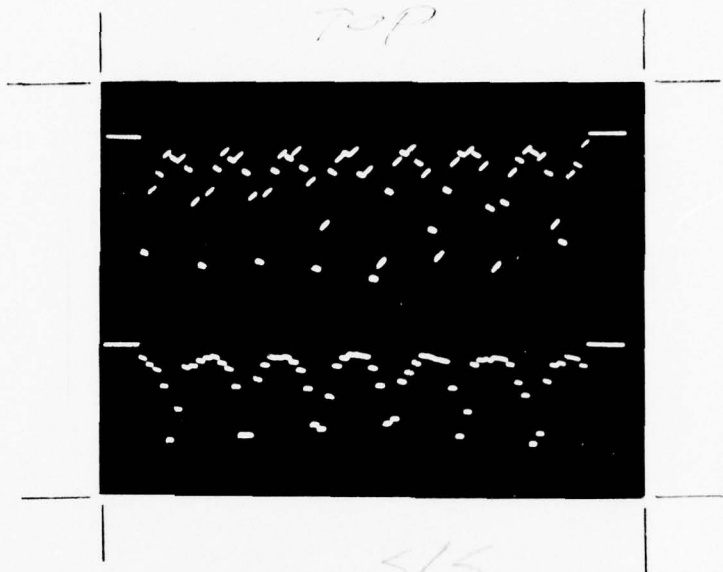


FIGURE 26. DATA WITH SOFTWARE FFT

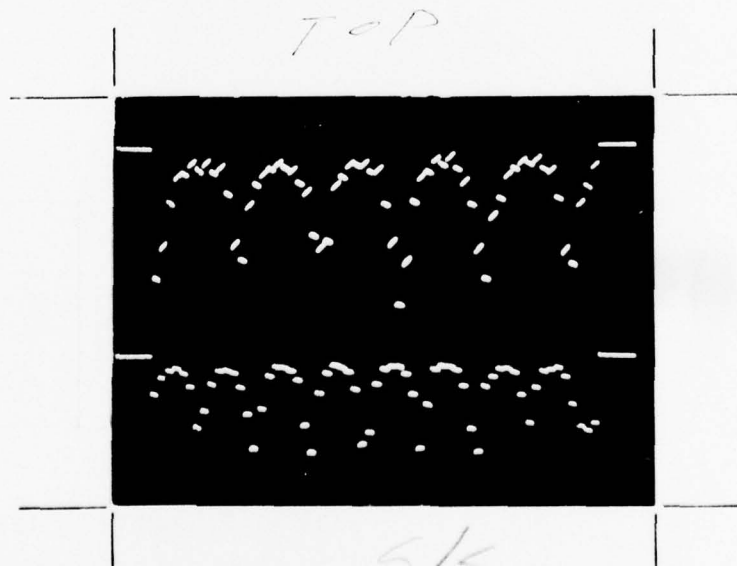


FIGURE 27 DATA WITH SOFTWARE FFT

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FIG-26+27
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OUTPUT ? X
FREQUENCY= +00002
+

OUTPUT ? Y
FREQUENCY= -00010
-

OUTPUT ?

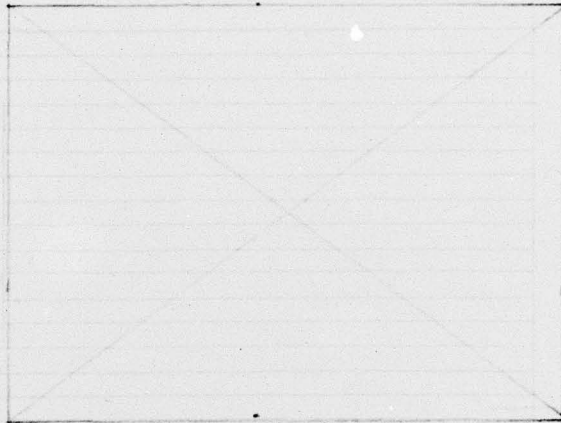


Figure 28. Data With Software FFT

LISTED ? Y

NO.# DATA AVERAGES , 1

OUTPUT ? Y

X-TOT SCAN DISTANCE ? , 1000

Y-TOT SCAN DISTANCE ? , 300

X-INCREMENT ? , 200

Y-INCREMENT ? , 100

X	Y	FREQ	LIST
00200	00000	LOW	226,001,001,001,005,001,002,001, 001,001,001,000,004,000,001,
00400	00000	0002	122,025,002,000,002,001,002,000, 001,000,001,000,004,000,001,
00600	00000	0007	065,009,010,000,001,001,026,009, 001,000,002,001,001,001,000,
00800	00000	0008	065,001,002,001,001,000,002,009, 001,001,002,000,001,000,000,
01000	00000	0007	050,001,001,004,001,001,005,004, 004,000,001,001,001,000,004,
00000	00100	LOW	200,004,001,004,001,001,002,000, 000,001,001,000,005,000,000,
00200	00100	LOW	197,000,001,001,002,000,001,001, 004,000,002,001,004,000,001,
00400	00100	0002	170,025,001,000,002,001,002,000, 001,001,005,000,001,000,001,
00600	00100	0007	050,001,001,004,001,009,037,000, 005,000,000,001,001,000,001,
00800	00100	0005	065,001,005,001,017,001,005,001, 005,000,002,001,001,001,001,
01000	00100	0006	050,004,002,001,002,009,005,004, 005,001,005,000,005,000,001,
00000	00200	LOW	122,002,002,001,002,001,002,001, 004,002,001,000,004,000,001,
00200	00200	LOW	170,005,001,001,002,001,000,001, 005,002,004,001,001,000,001,
00400	00200	LOW	170,004,001,000,002,001,002,001, 001,000,002,000,000,000,001,
00600	00200	0005	085,004,001,001,017,016,002,001, 002,000,005,000,001,001,000,
00800	00200	0006	082,001,005,000,005,025,001,000, 005,001,005,000,000,001,001,
01000	00200	0007	082,001,002,004,001,000,009,001, 004,001,000,004,004,000,001,
00000	00300	0011	082,004,005,000,001,001,001,001, 001,000,005,000,001,001,000,

Figure 29. Finalized Data Run. Sample

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Figure 30: a-r gives a comparison between the data incident on the detector and the data plots from the exit lines of the scanning detector, monitored on an oscilloscope. The top line of each plot is a detector scan in the x-direction and the bottom plot is a detector scan in the y-direction. It is left to the reader to interpret the results.

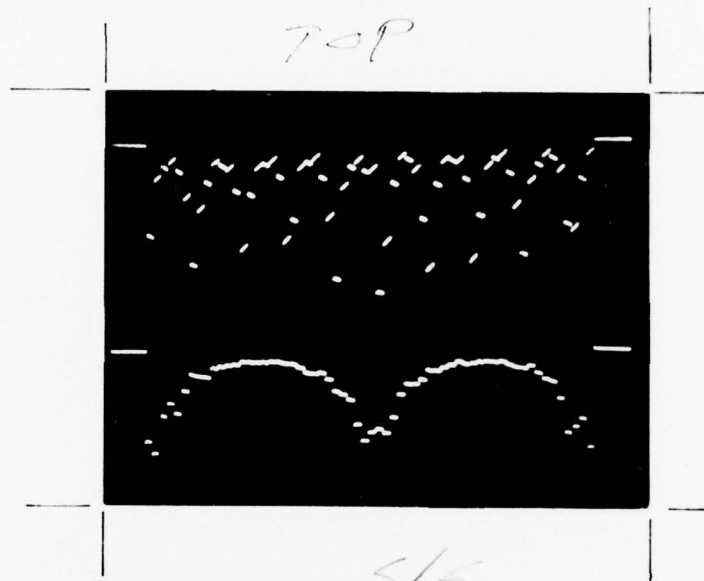


FIGURE 28. DATA WITH SOFTWARE FFT

AFAL-TR-77-203
FIG-28
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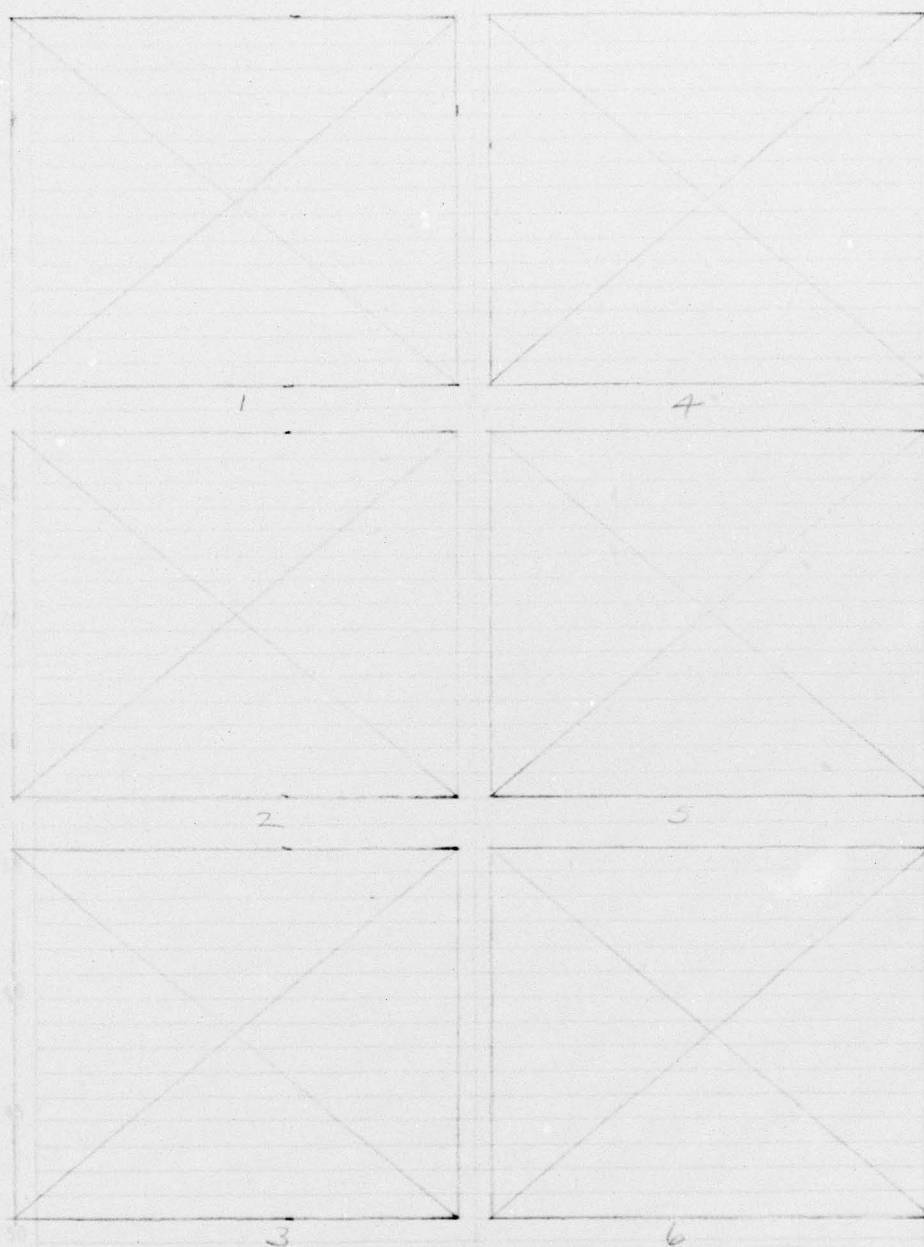


Figure 30 (a-c). Real Data With Different Specklegram Outputs

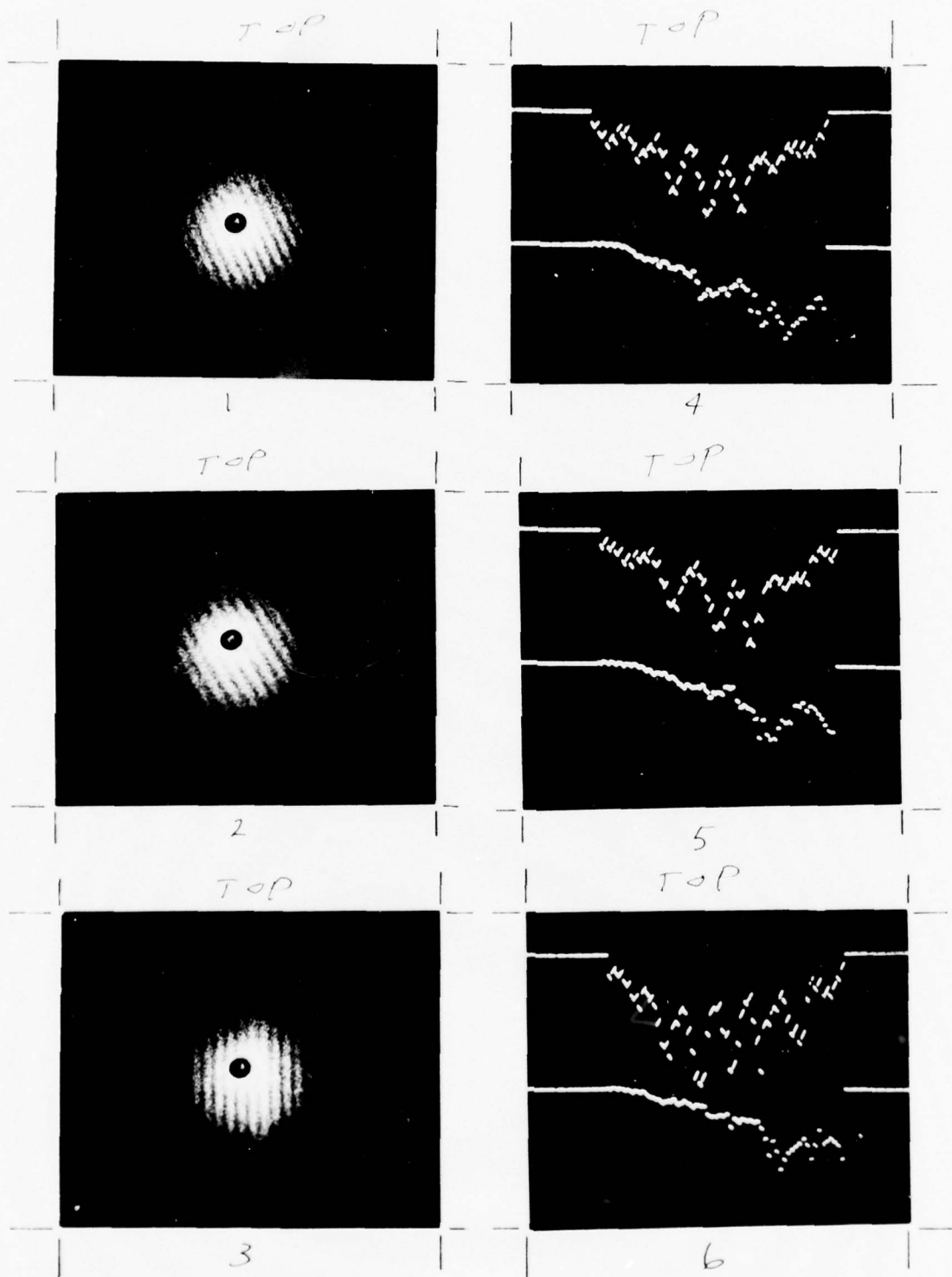


FIGURE 30. a - c

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FIG-30.a-c

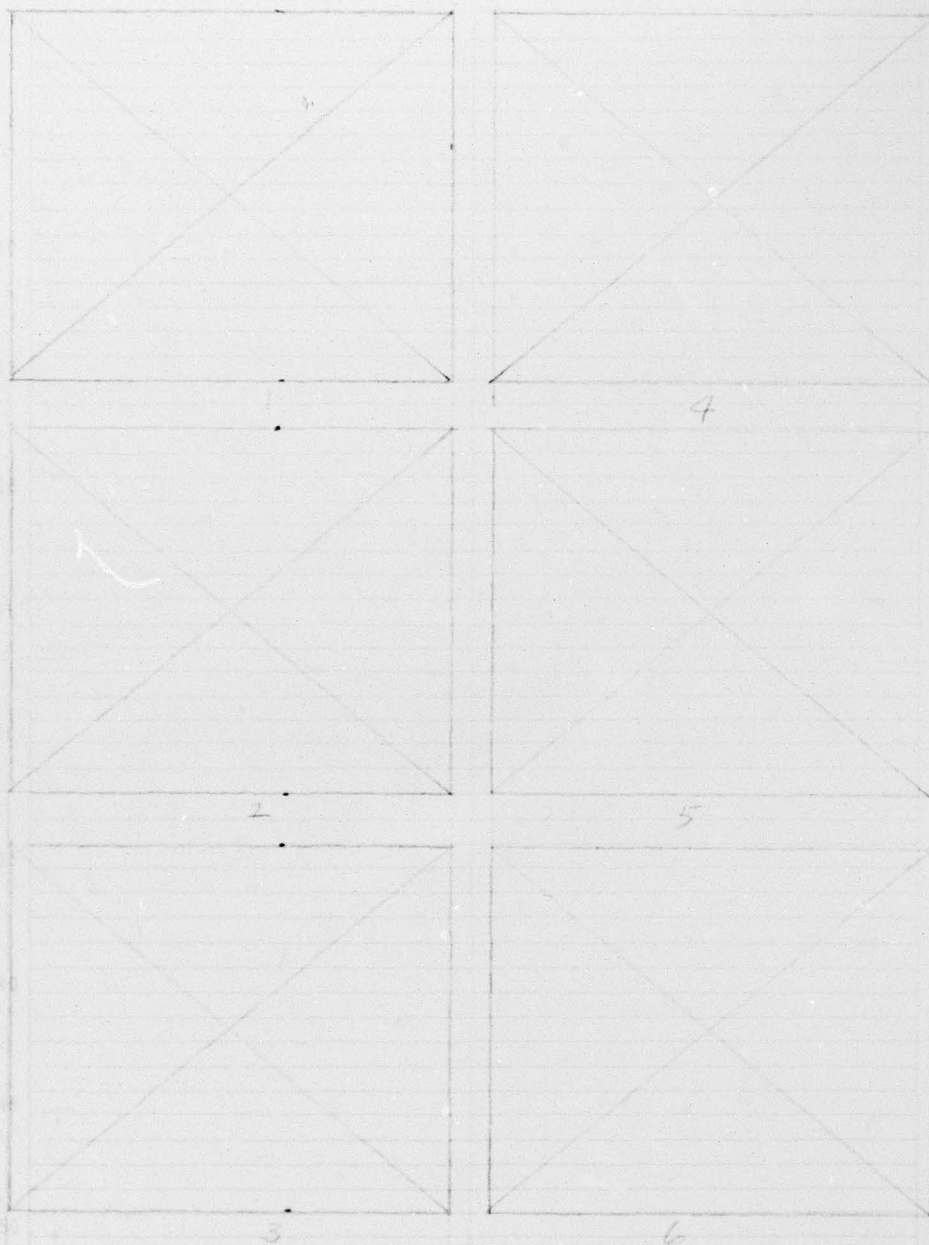


Figure 30 (d-f). Real Data With Different Specklegram Outputs

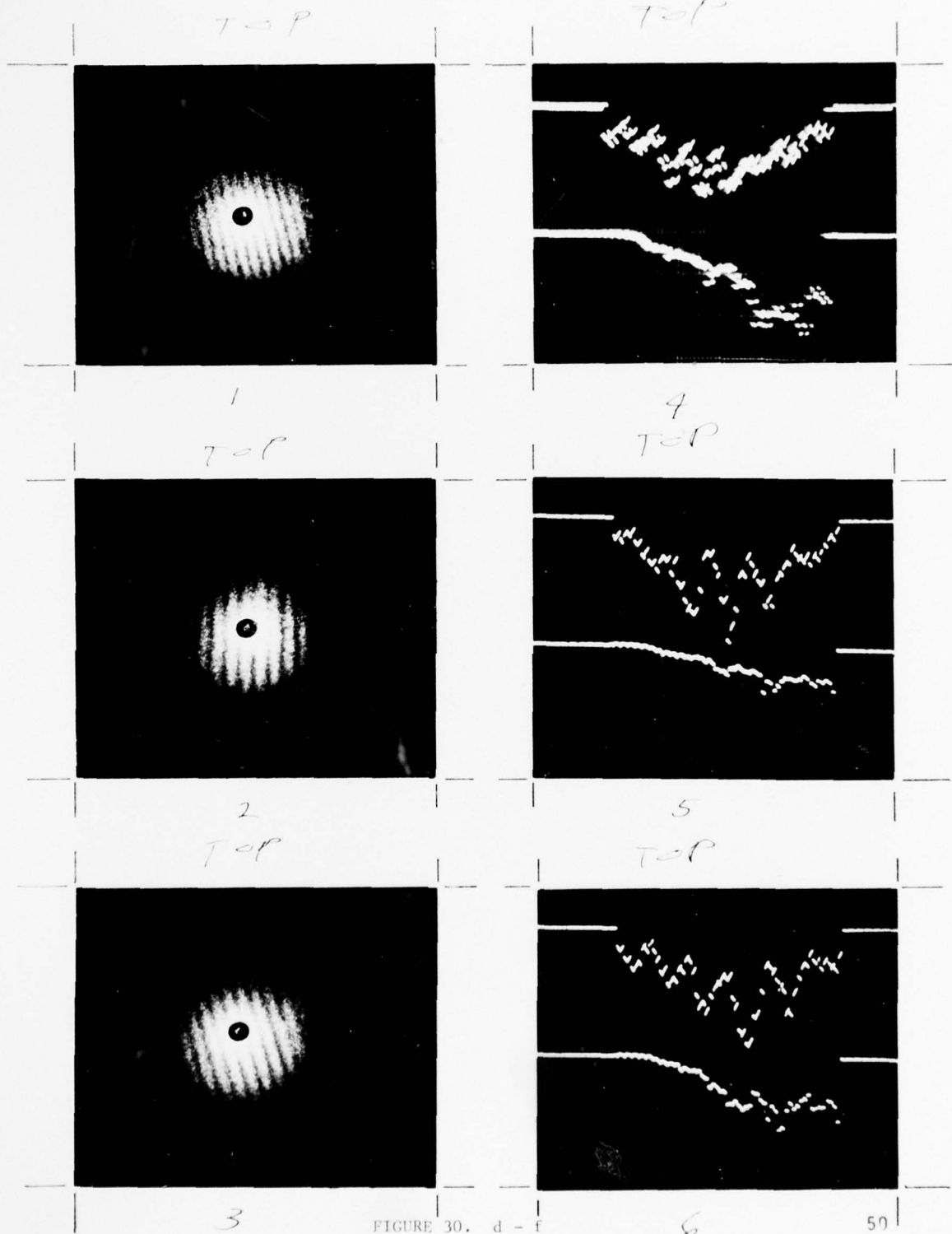


FIGURE 30. d - f

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 HFM-TR-77-203
 FIG-30. d-f
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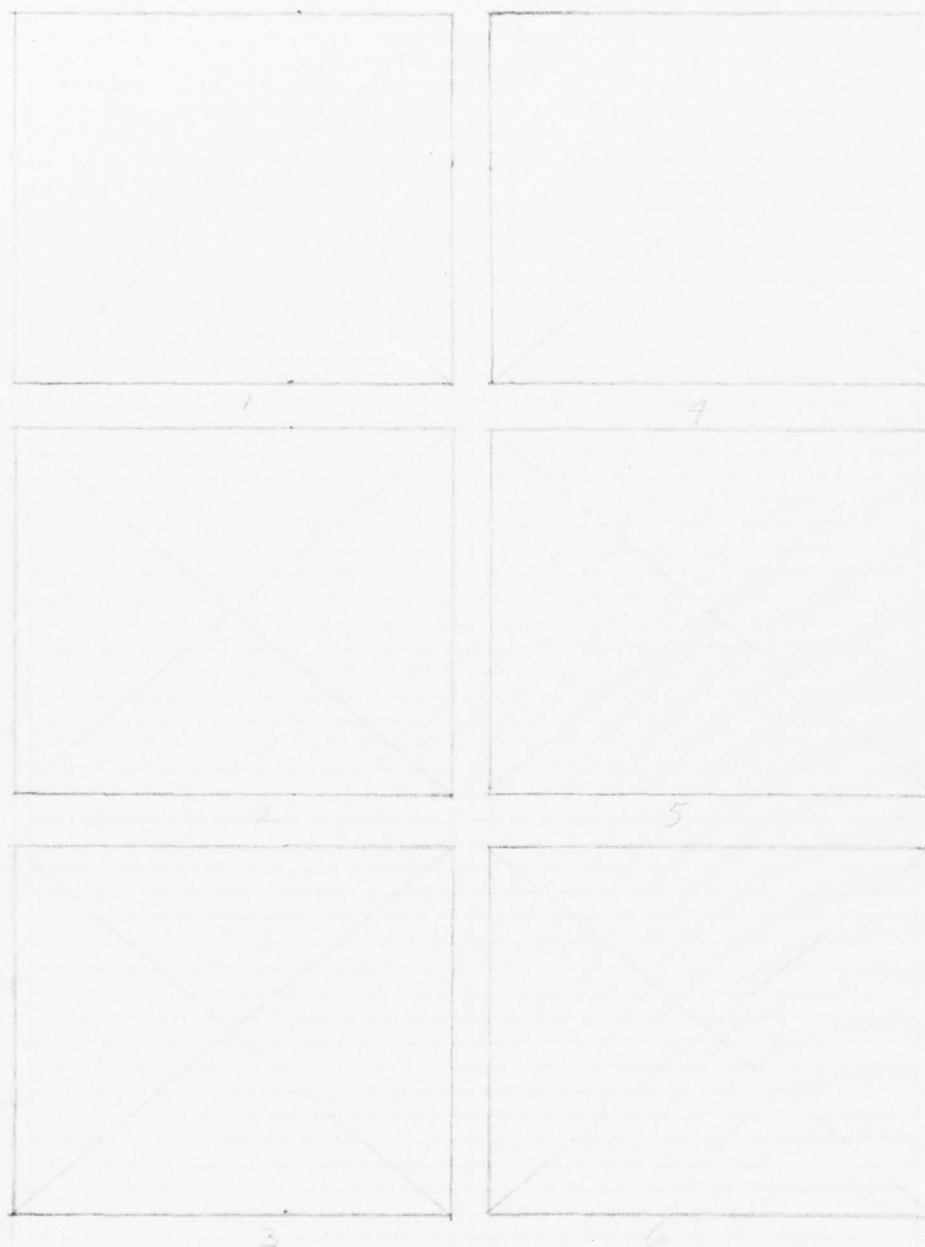


Figure 30 (g-i). Real Data With Different Specklegram Outputs

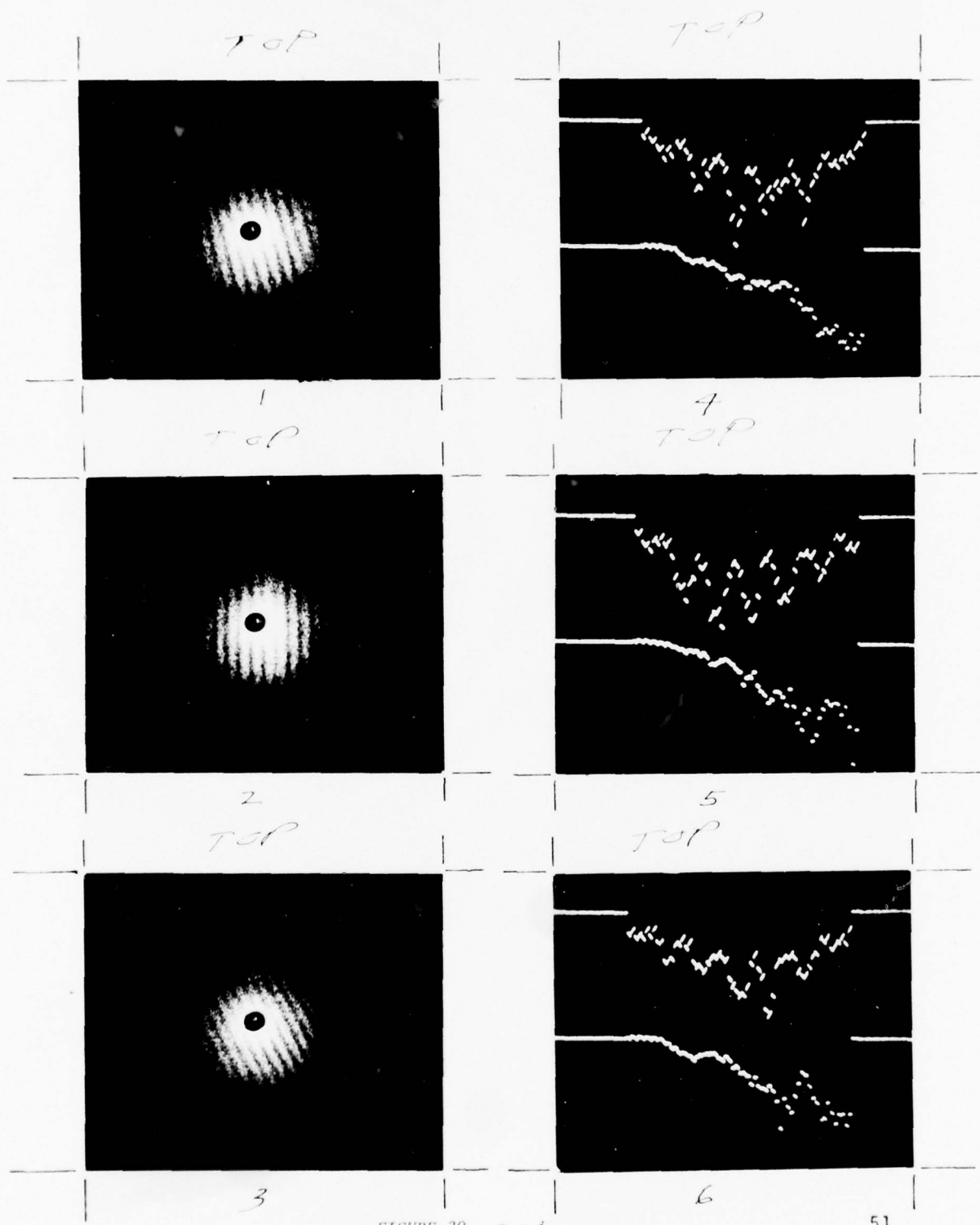


FIGURE 30. g - i

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 FIG-30. g-i
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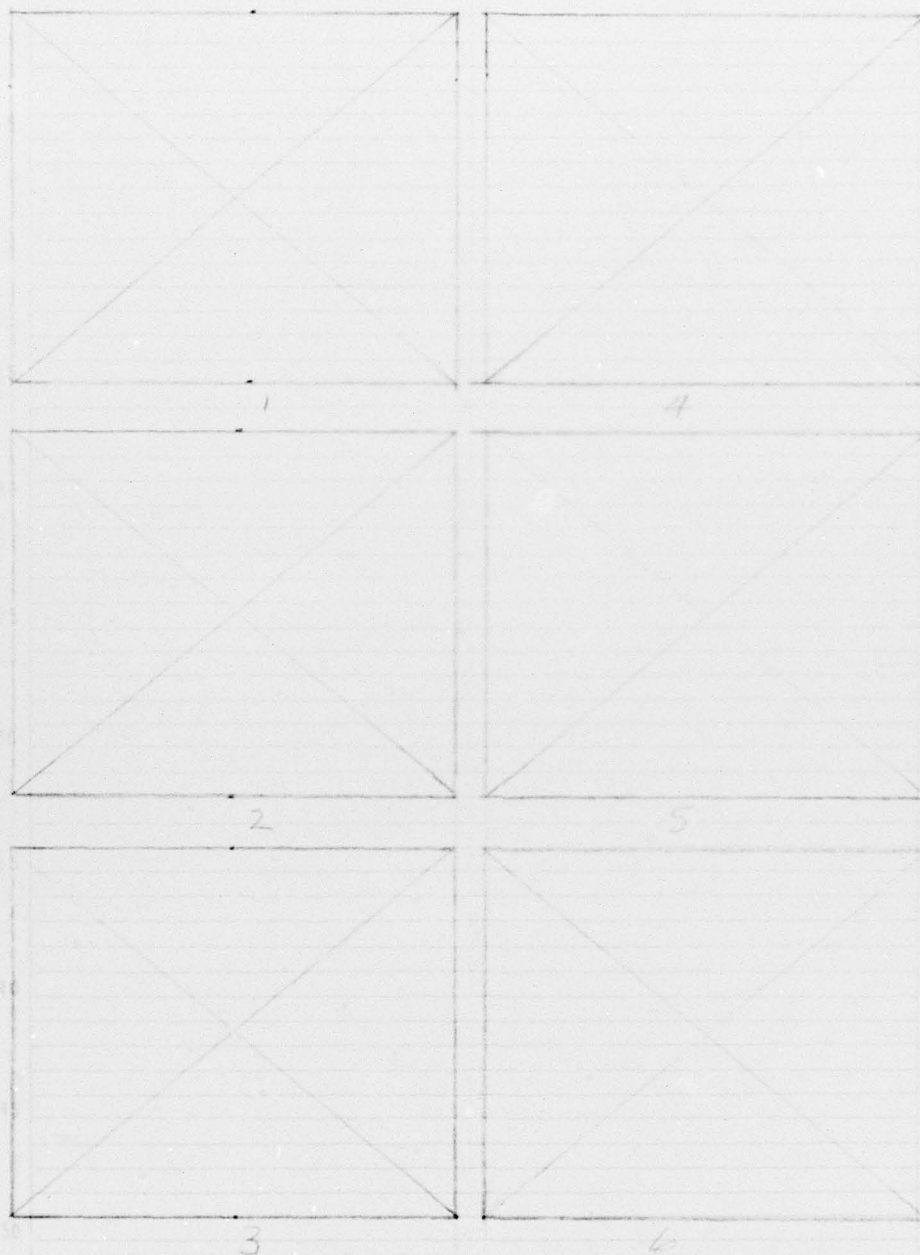


Figure 30 (j-1). Real Data With Different Specklegram Outputs

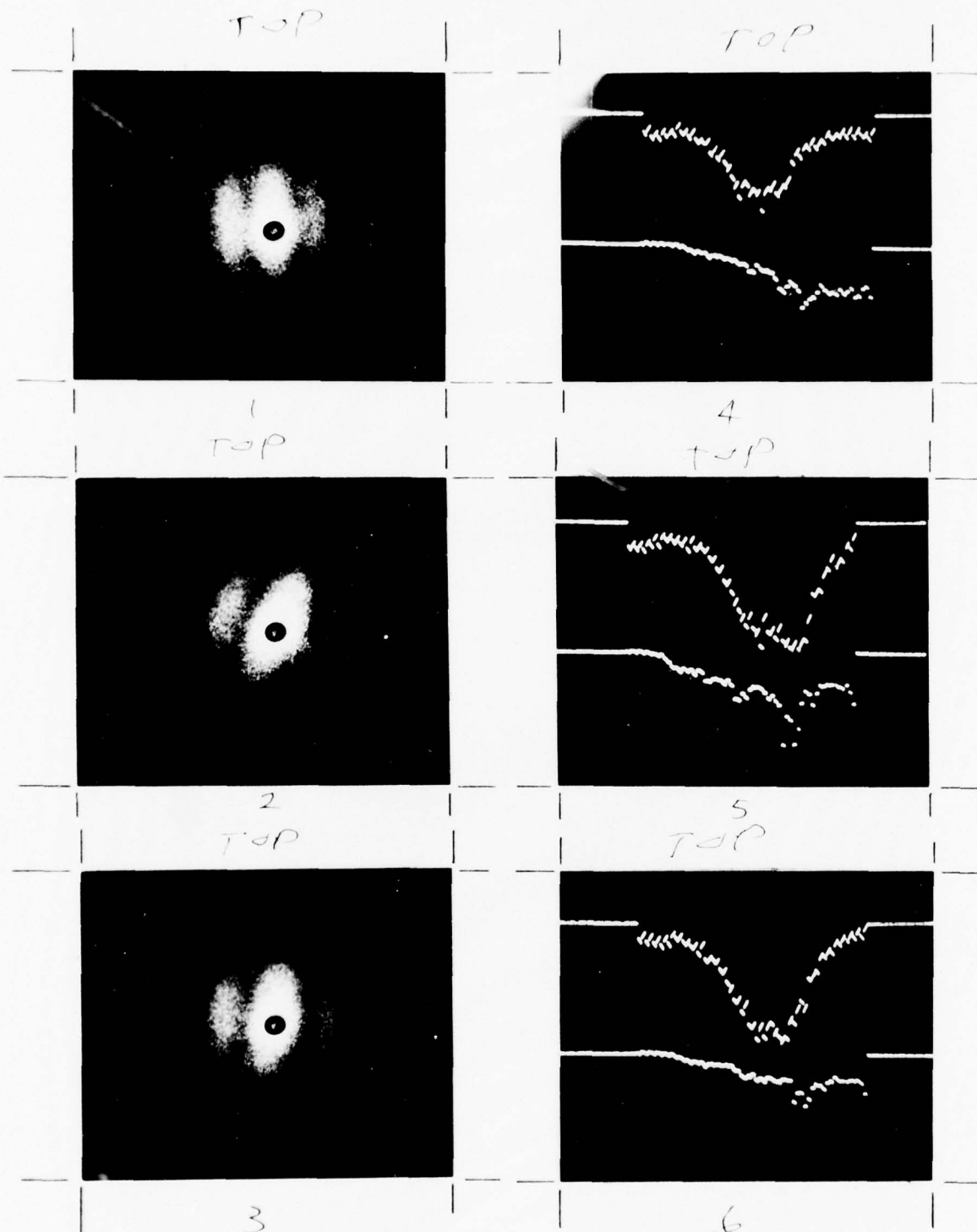


FIGURE 30. j - 1

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FIG- 30. J-L

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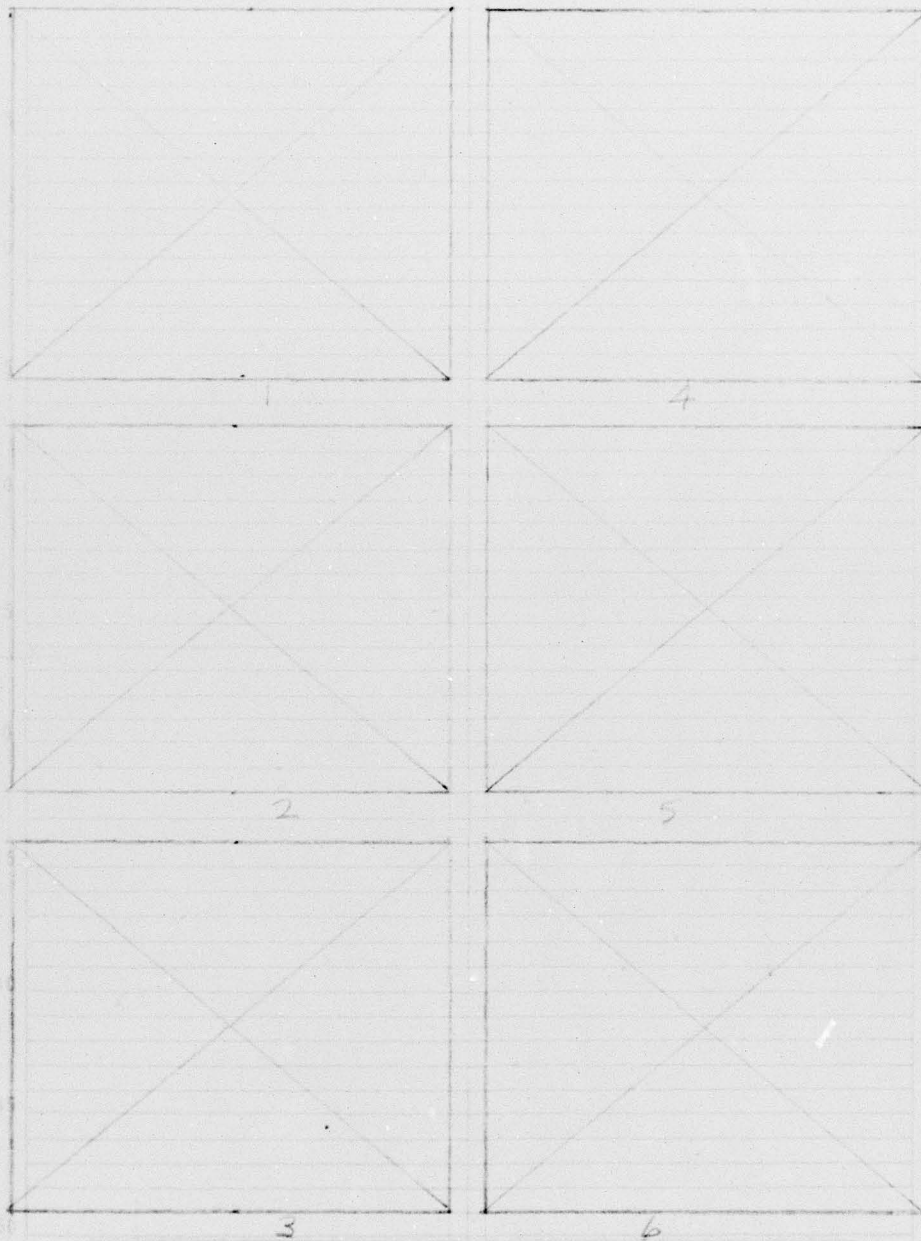


Figure 30 (m-o). Real Data With Different Specklegram Outputs

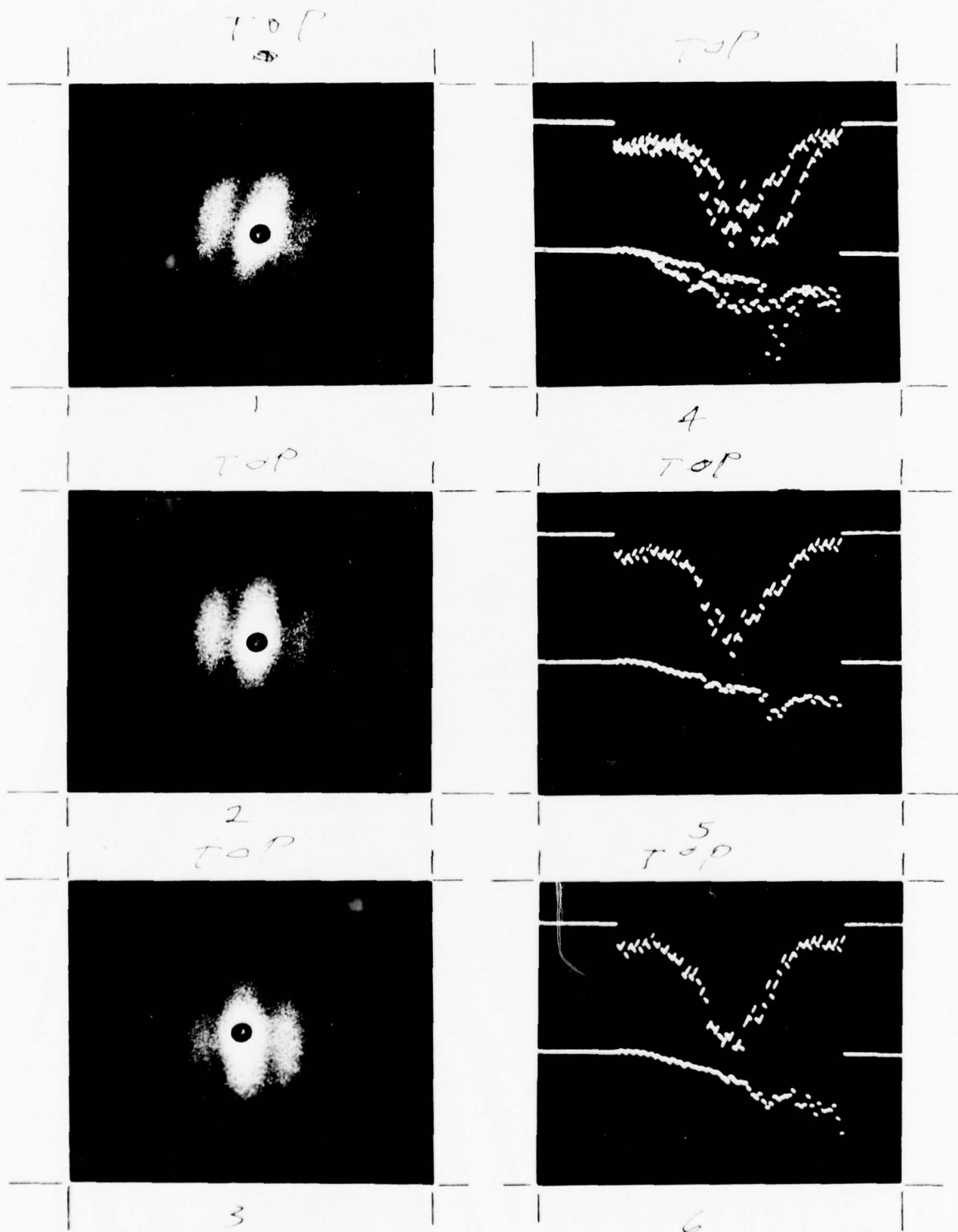


FIGURE 30. m - o

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 AFAL-TR-77-203
 FIG-30. m-o

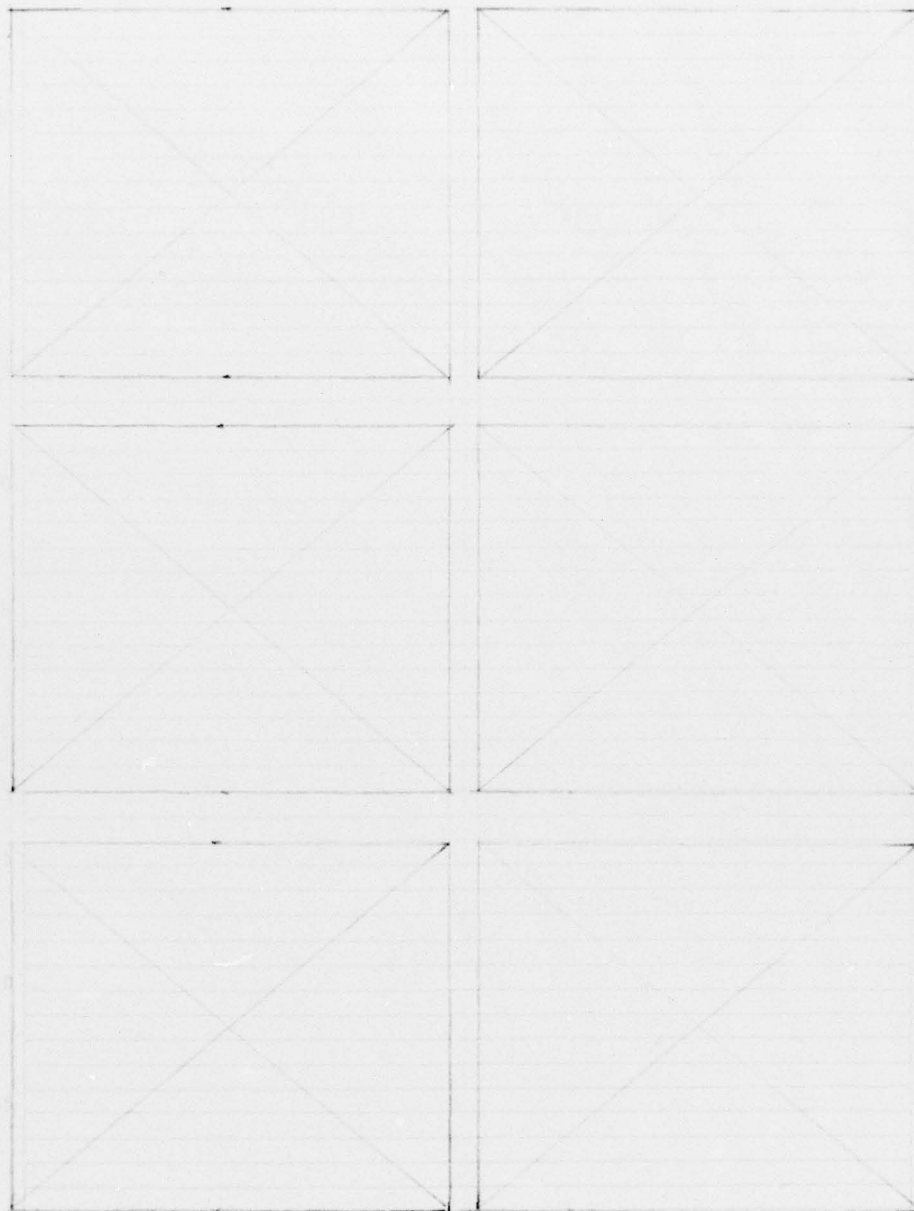


Figure 30 (p-r). Real Data With Different Specklegram Outputs

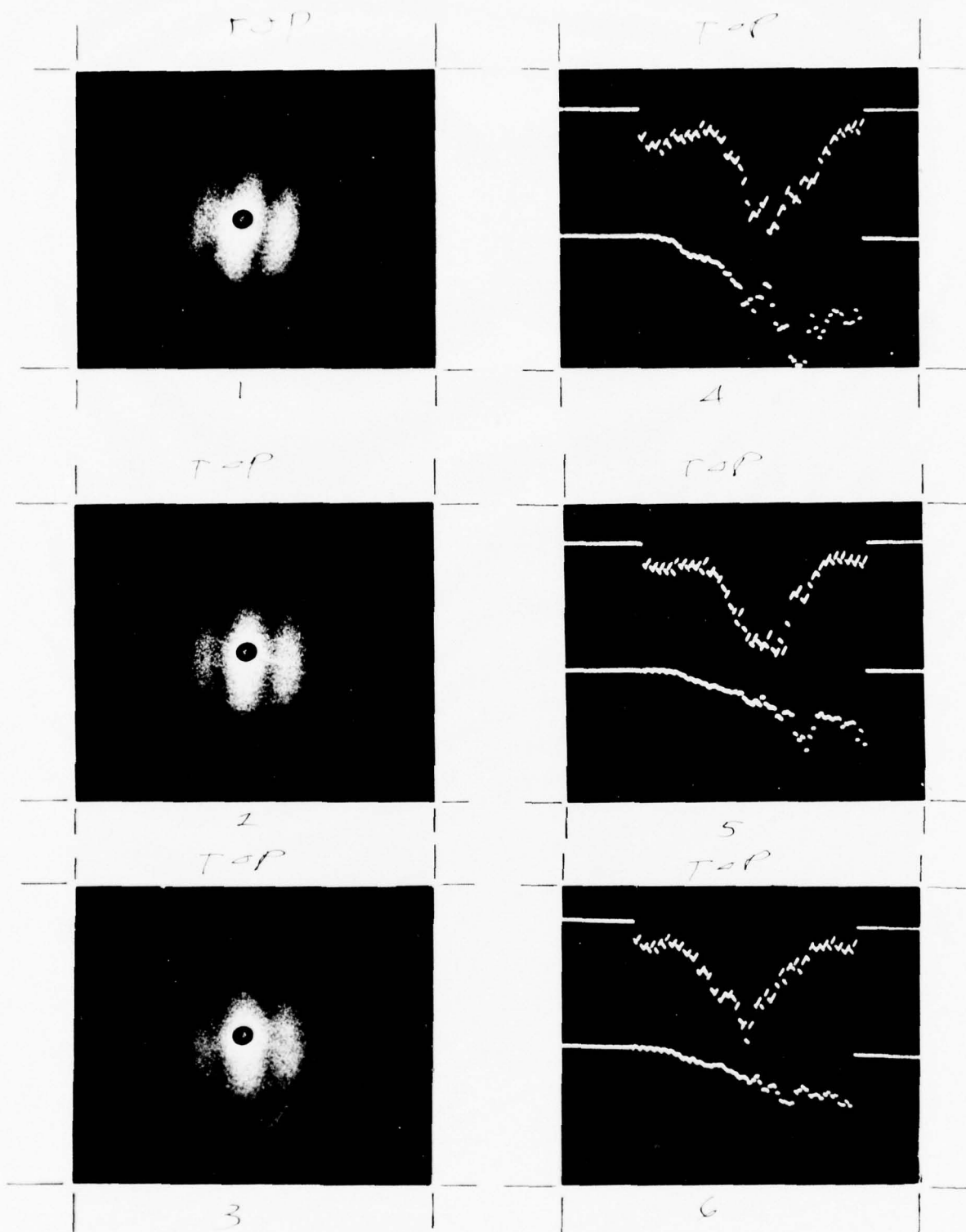


FIGURE 30. p - r

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 11/AL-TR-77-203
 FIG-30. P-R
 DATE-53

SECTION VII

RESULTS

The results, although they did not meet the original requirements, produced some meaningful information as well as some aid toward development of a system to solve some of the problems of specklegram readout for the Air Force Flight Dynamics Laboratory.

The discussion that follows in this section pertains only to the system as it exists in its present state of development, directing itself in a time ordered fashion from the program beginning to now.

Much time was spent at the start in generating the correct electronics control signals, through the specially built logic circuitry, for activating the x-y stepping stage and the two dimensional detector array. Many capacitor and resistor changes were experimentally adjusted to allow the proper amplitude and pulse widths of the driving pulses required to operate these peripheral units optimumly.

Almost fifty hours of machine shop time was required to build the hardware to integrate much of the equipment. For instance, a specklegram holder had to be built for mounting to the x-y stage, a base was constructed to mount the x-y stage to the optical bench, a base was built for mounting the detector, and some special hardware was constructed for rack mounting the electrical circuitry and labeling the faceplate.

The system was then assembled and checked out in its final form as satisfactory and operable.

The software required most of the time from this point on. Each subroutine discussed in the software section of this report was written and rewritten until a final workable program was achieved. The data analysis section of the software program was written in two different forms: 1.) peak detection, 2.) Fast Fourier Transform. Essentially all the software for the peak detection was thrown out after it was determined to be inadequate for data analysis. Nearly all of the software progressions for both methods will be available at the contract close-out time.

SECTION VIII

CONCLUSIONS

In this section, I would like to discuss the present capability of the final system and also interject some possible solutions toward establishing a more accurate and feasible system for carrying out the initial objectives laid out for this project.

It appears that most of the objectives such as data analysis speed, automatic data input with .001-inch accuracy, and fringe angle and spacing determined by nonmechanical means, have been achieved with relatively few problems. It has been demonstrated that: 1.) a data analysis rate of 1-2 Hz is feasible in the existing software system; 2.) a .001-inch accuracy of stepping positions can be achieved under computer control at the above data analysis rate; and 3.) the detector scheme of two orthogonal linear arrays allows for the determination of angle and displacement completely independent of the fringe orientation on the detectors.

After completion of the software preliminaries and a checkout of the FFT portion of the computer program, some of the specklegram data furnished by Flight Dynamics Laboratory, was introduced for initial tests. During the testing period, various optical configuration changes were made such as varying the size of the readout laser beam and changing the image size of the specklegram fringes on the detector faces, which compensate for noise and detector optimization respectively. It was found that a beam size of approximately .25 mm was optimum to give maximum fringe contrast yet not cause too high a noise level due to large secondary speckle. It was also determined that an image size about 1-1/4 times the detector length utilized the detectors to their fullest, maintaining the best ratio between number of detectors per fringe and number of fringes per detector. For example, if 15 fringes were present across the complete halo, then approximately 12 fringes would be imaged across the 64 detector elements; thus there would be 5-1/3 detectors per fringe. For a low number of fringes (5) there would be 4 fringes projected onto the detectors thus 16 detectors per fringe.

The best results that could be obtained from the 15 fringe case would be to the nearest fourth of a fringe but since noise and other experimental errors are present, only about 1 fringe resolution can be obtained. For the case of 5 fringes in the projected halo, about a quarter of a fringe resolution is possible. The system, as it exists in its present state, can analyze data at a 2-3 point per second rate with a very low resolution accuracy.

Some thought has gone into methods of improving the system resolution which appears to be the main problem at the present time, without any major change in the overall system configuration.

The first thought which came to mind was to try to reduce the secondary speckle noise without changing the fringe resolution of the output data. Two methods of in-house experimentation are going to be performed for solving this problem. The first will be to slightly misdirect, at a high fringe rate, the readout laser beam in an optical system where the image plane is held stationary. This could be performed with a motor driven rotating wedge. The second method would be to project the output fringe pattern onto a liquid crystal dynamic diffuser, which acts as a random phase medium that is electrically controlled. A surface of this type would tend to shift the secondary speckle a small amount in a random fashion at a rapid rate. In both the above mentioned methods, the secondary speckle noise would be minimized by taking several detector scan data samples and averaging them digitally over a short period of time. This process could be done with a small amount of modification to the existing system.

Another way of analyzing the specklegram data that will be considered, uses the optical fourier transform. By using either the rotating wedge or the diffuser as a noise reduction scheme, an optical system consisting of a laser, specklegram, diffuser, fourier transform lens, D.C. Block, and appropriate detector could perform the equivalency of the digital fast fourier transform operation, in an optical train with an essentially zero time frame, thus eliminating one large time consuming aspect of the present method.

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All of the above techniques are being considered in-house under project 2001-02-42 of AFAL/DH0-2. If any of the methods prove feasible then further experimentation could be performed by Flight Dynamics Laboratory approval.

APPENDIX I

A FEASIBILITY STUDY OF AUTOMATIC FRINGE COUNTING TECHNIQUES

13 November 1973

By C. Richard Lane

BACKGROUND:

As a result of structural problems associated with the C-5 aircraft, Dr. Lovelace has asked that all laboratories reflect on possible solutions to the problem of monitoring the structural integrity of critical areas on the aircraft. Based on their past experience in the area of non-destructive testing of aircraft structures, Flight Dynamic Laboratory organized an approach to provide such a monitoring system in cooperation with ARL, and AFAL. This work is presently being done under AFFDL work unit 1467-02-12 with Mr. Gene Maddux and Dr. Frank Adams as principal investigators.

The initial approach taken by FDL utilizes the recording of a double exposure speckled image of the area of the structure being monitored, where some strain is introduced between exposures. This double exposed image is then processed to make a transparency. Upon illumination by a small laser beam a set of fringes are projected which represent the correlation of the speckles at that location on the image.

These fringes can be related to the surface motion that took place between the two exposures, the structural integrity at that point.

Although this technique is limited with respect to the size, type, and depth of the flows that it can detect, it provides a good first step and is essential to more complex techniques that have potential of overcoming these limitations.

For each C-5 aircraft a large number of these specklegrams would be required (5,000 - 10,000 if one specklegram were made for each installed wing fastener) and a large number (100 - 1000) of points per specklegram would need to be analyzed. It is, thus, obvious that an automated system is required that will map the surface motion with each specklegram area.

OBJECTIVE:

The objective of the initial in-house effort within AFAL was to investigate techniques of determining the spacing and direction of a projected sample fringe pattern. This investigation included the demonstration of the techniques on a sample specklegram provided by AFFDL.

APPROACH:

As a result of past experience with similar type problems in the area of optical processing and the availability of equipment within AFAL two approaches to the problem were taken. Both approaches required that the fringe pattern be read-in automatically by one of three ways:

- a. Scanning point detectors.
- b. Electrically scanned linear diode arrays.
- c. Electrically scanned 2-dimensional image, dissector tube.

Once the fringe information was detected, two approaches were considered to analyze the fringes and indicate the spacing and direction. The two approaches were:

a. Store the information in a memory unit, then perform a 2-dimensional fast fourier transform (FFT) to determine the spatial frequency component in both magnitude and angle. The FFT was chosen over optical transforming due to the lack of spatial coherence in the speckled fringe pattern.

b. As the information is read-in, perform a peak detection operation and average the peak spacing for scans in two directions. By means of a simple arithmetic operation the maximum spacing and direction were then determined.

Evaluation of both approaches were carried out on the sample provided.

DISCUSSION OF THE 3 DEMONSTRATION TECHNIQUES:

Two of the three demonstrations to be discussed now were done only minimally and were investigated only to the extent of being considered as a possible solution to the fringe counting problem. Although all three demonstrations were capable of providing a solution to the problem, only the third was experimented with to the desired extent. It will also be seen that the 3 demonstrations were similar enough in theory that it can be assumed that if one experiment works then all three, with proper implementation, can serve as a solution. All three techniques have been discussed and demonstrated to: Mr. G. Maddux and Dr. Frank Adams of the Flight Dynamics Laboratory.

1) On 6 August 1973 a sales representative from Tektronix Incorporated accompanied to our lab, a processing oscilloscope being considered for purchase under project 2001-04-10. The sales representative set up the processing system in the lab which consisted of a Model 7704A

oscilloscope with standard scope plug-ins, a Model 7001 Processor, a PDP 11-05, 16K core mini-computer, a CRT display terminal, and a rapid read-write tape punch. The self-scanning detector array was introduced into the system through the oscilloscope inputs. The array, scanning its 512 elements at a 200 Hz rate, was synchronized to the scope such that all 512 elements were displayed on the scope screen in one sweep (5msec). The processor portion of the system then digitizes the data displayed on the scope screen and sends it to the PDP 11 computer along with a command of which software program to implement on the data. The resulting answer can then be displayed by a curve trace on the scope screen or CRT screen of the terminal.

Due to a lack of time and the limited software programs available by the sales representative, only a fast fourier transform program was used to attack the fringe counting problem. The fringes to be measured were imaged on the reticon array and displayed on the scope. By a stroke of luck, the FFT program being demonstrated needed 512 digitized points to perform the transform, exactly the number of detectors in the scanning array. The signal being displayed is now averaged over several scans of the array and then the FFT program is called up and performed on the averaged signal and the result displayed with 512 points on the oscilloscope screen.

Two sets of fringes were experimented upon during the demonstration: An equally spaced set of .05 inch fringes; and a set of fringes generated from a specklegram.

a. Figure 2a shows the fringes imaged on the reticon and averaged 1024 times to eliminate unwanted noise. From the figure there are 21-22 fringes across the 512 elements of data, and multiplying the number of fringes by 200 Hz (the scan rate of the detector), gives the frequency that the computer actually sees.

$$(1) \quad 21 \times 200 = 4200 \text{ Hz} = 4.2 \text{ KHz}$$

$$(2) \quad 22 \times 200 = 4400 \text{ Hz} = 4.4 \text{ KHz}$$

Figure 2b illustrates the fast fourier transform of the signal of Figure 2a, and the strong peak (arrow) is printed out as 4.3 KHz, a reasonable result.

b. Figure 3a is a scope trace of a sample specklegram from FDL, one trace a single sweep and the other a trace averaged 512 times. These two traces illustrate the noise reduction capability of averaging a signal over several traces. This noise reduction factor could prove very necessary if other methods of fringe counting other than FFT, is implemented. The FFT displayed in Figure 3b shows two significant peaks of data relating to the fringe spacing. The peak indicated by the red arrow is a 200 Hz frequency spike representative of the scan rate of the reticon array. This frequency spike is a consequence of the input fringes not filling the entire aperture of the array, thus the synchronizing pulses from the clocking circuit of the array are prominent. If approximately the first 30 registers of the data in Figure 3b are set to zero (200 Hz spike), the strongest frequency then becomes the second spike and this frequency value is printed in Figure 3c with a 50mv to 20 mv vertical scale change. By examination of Figure 3a it should be obvious that 4.2 MHz represents the fringe frequency of major concern. As a simple conclusion, a software programming addition that cancels out the 200 Hz clocking rate would be incorporated and only the desired frequency peak would be predominate. By retransforming the result obtained in Figure 3c, it is seen that the same fringe spacing is preserved after cancellation of the 200 Hz peak (Figure 3d).

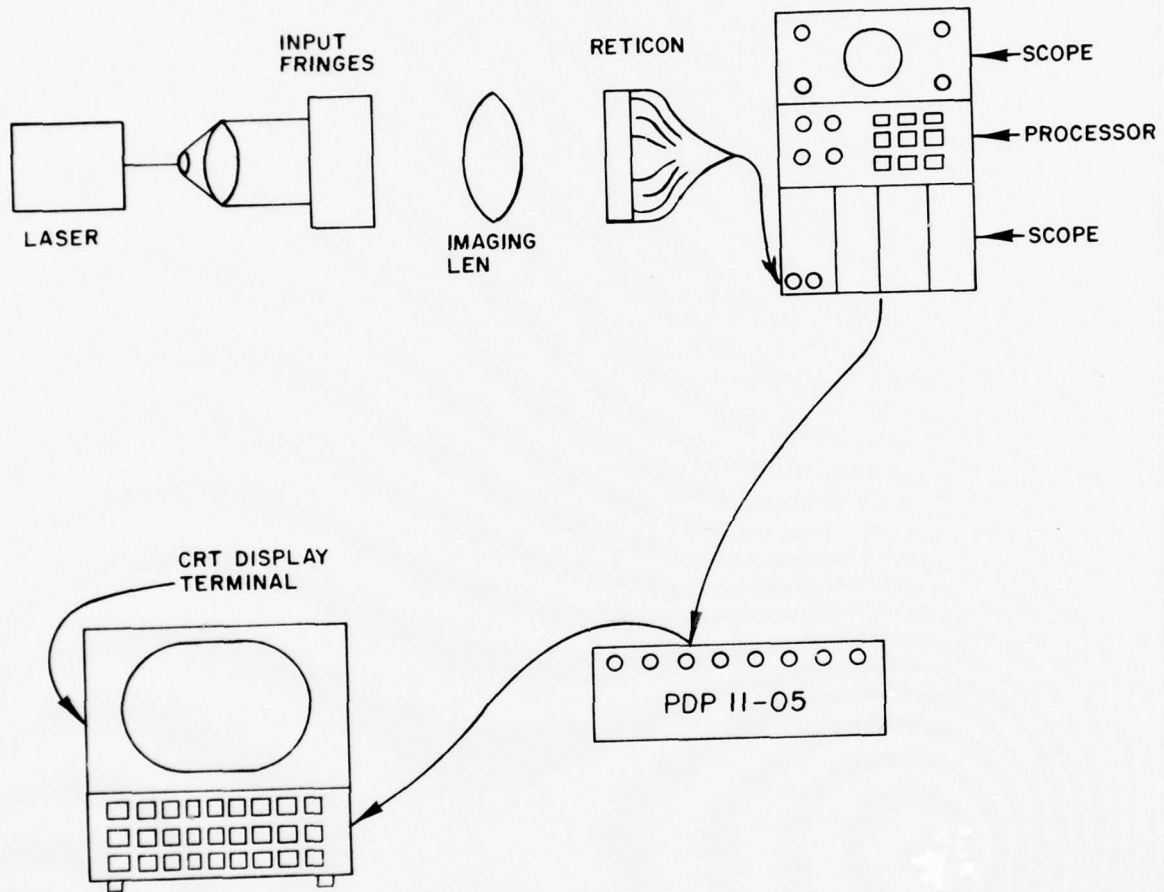


Figure 1a

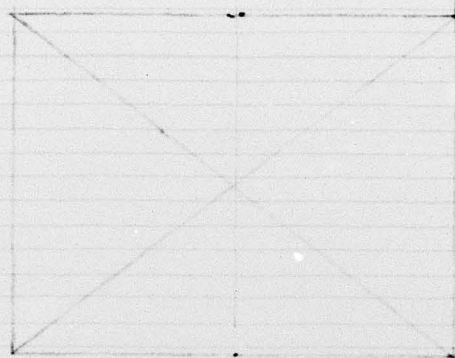


Figure 2a

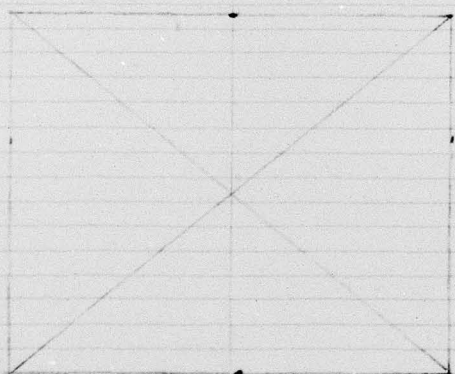
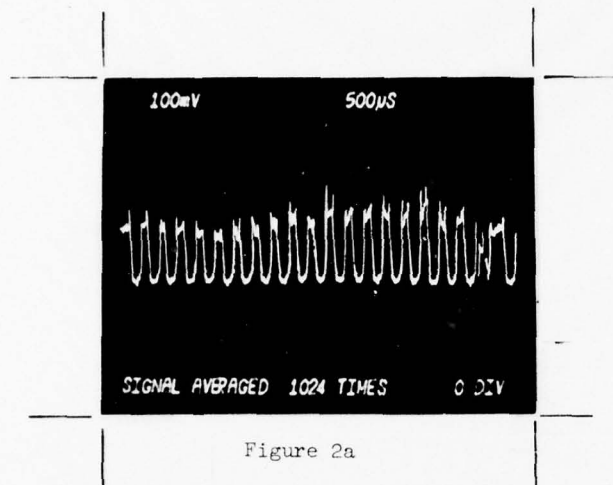
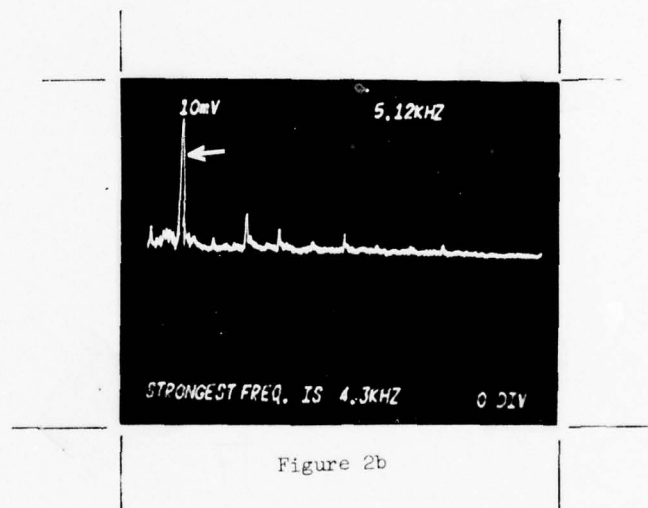


Figure 2b



S/S



S/S

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FIG-23+20

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2) The second method of demonstration will be discussed only briefly since it is similar in procedure to the third demonstration with slightly more sophisticated equipment. Figure 1b shows the basic setup used for this demonstration. The primary difference between this procedure and the first demonstration procedure is that instead of calculating a fast fourier transform with a PDP 11 computer, a counting program was implemented. The program performs an adjacent register comparison to locate peak points and then checks the difference between these peak points. This approach is instrumented by two orthogonal scans across the fringe pattern with an electronically raster scanned image dissector tube. Essentially, the result is an x and y fringe spacing measurement of which an actual fringe spacing may be calculated along with a fringe angle displacement. This procedure will be discussed more thoroughly in the next demonstration. The sole purpose of this experiment was to indicate the feasibility of using an image disector tube for the fringe counting problem.

3) The demonstration to be discussed now utilized equipment already existing in the laboratory of AFAL/TEL and thus was readily available during a longer period of time required for a more thorough investigation. The equipment used and its configuration are illustrated in Figure 1c.

SYSTEM DESCRIPTION:

A laser is used to illuminate a set of fringes at the input plane and an imaging lens projects the fringes onto an x-y scanning aperture. The variable size aperture is scanned by two bi-directional variable speed D.C. motors which are manually started and stopped. The aperture sizes are configured such that the resolution of the system can vary from a small fraction of one fringe down to a single fringe or essentially no resolution. This aperture size variation can be used constructively to reduce noise in the system resulting in less software work and time for the computer to implement at a later stage in the processing. A digital

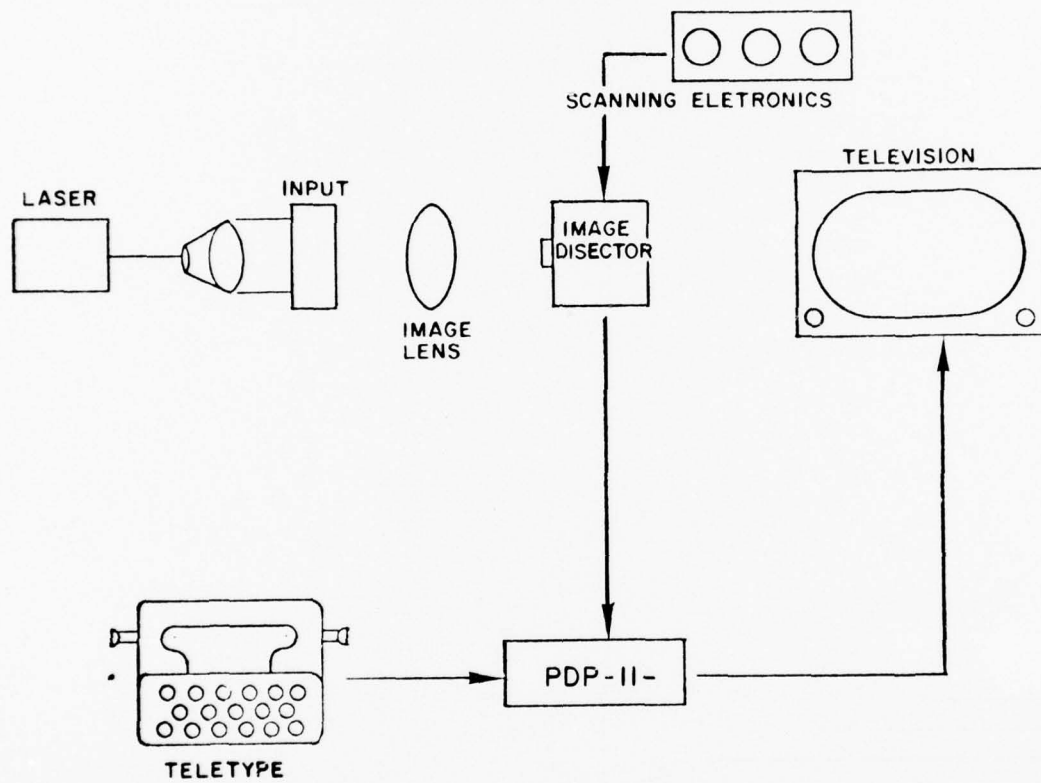


Figure 1b

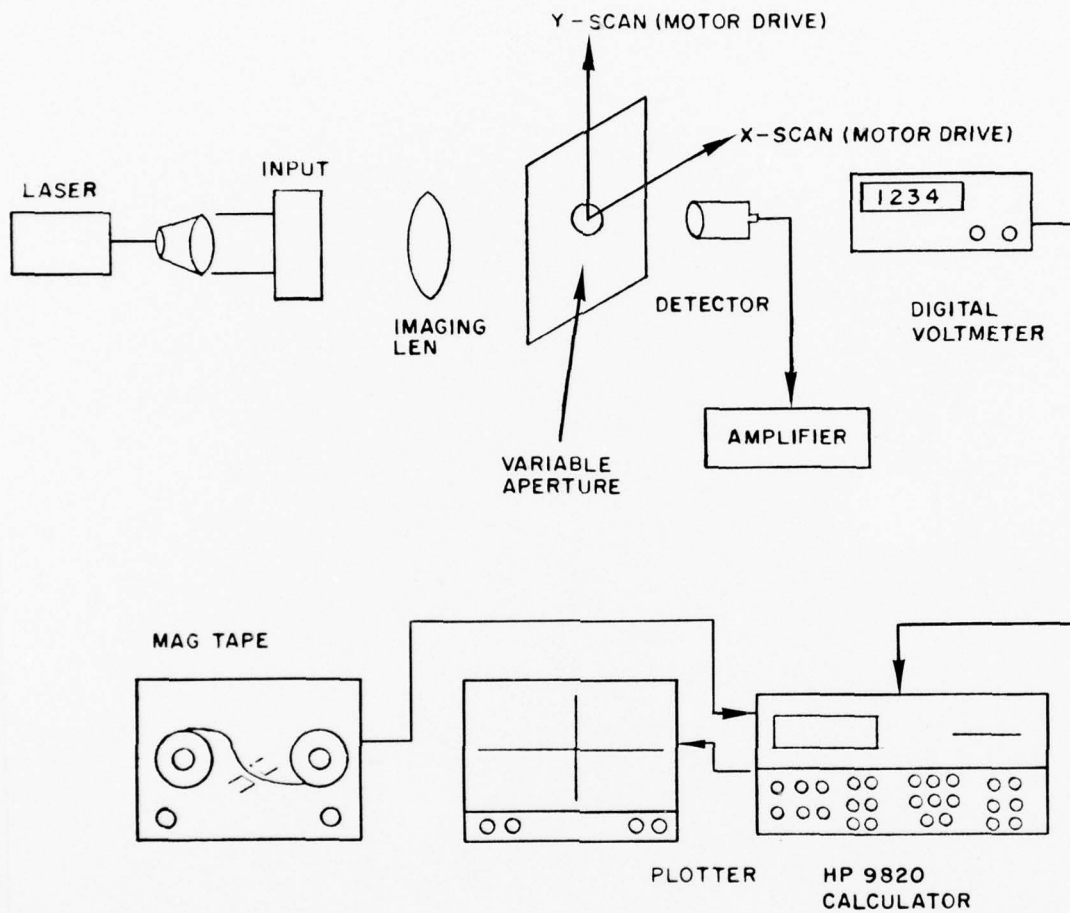


Figure 1c

voltmeter is used to pick up the intensity pattern of the fringes and also serves as an analog-to-digital converter that directly interfaces with the Model 9820 Hewlett Packard Calculator. The digital voltmeter and calculator combination is extremely slow for use as a data collector since it operates at a maximum data sampling rate of 3 samples per second. This fact rules out this type of system as a final product to solve the fringe counting problem, although it strongly demonstrates the feasibility of using a similar fringe counting technique with a data reading capability of approximately 4-5 magnitudes greater. A plotter can also be tied directly to the system giving a visual description of the fringe data that the calculator will process.

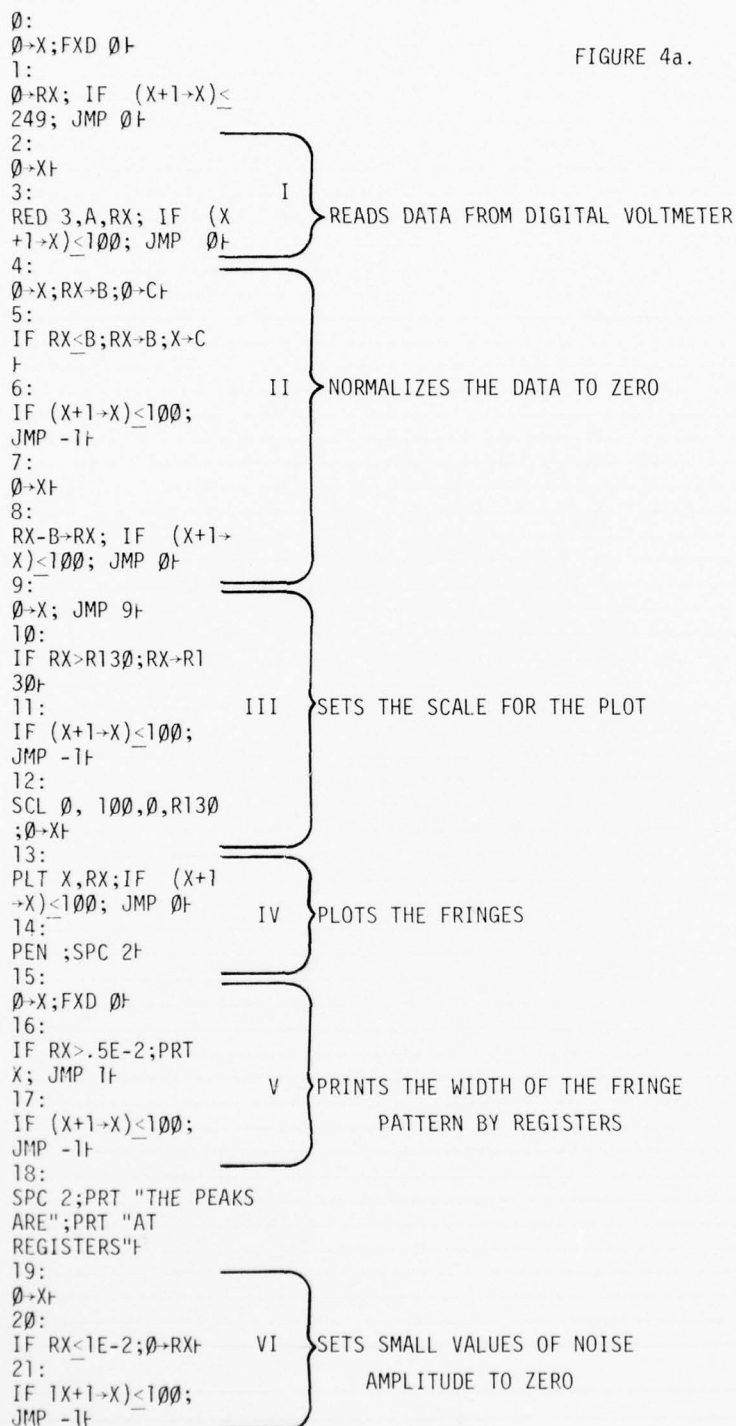
SAMPLE PROCEDURE:

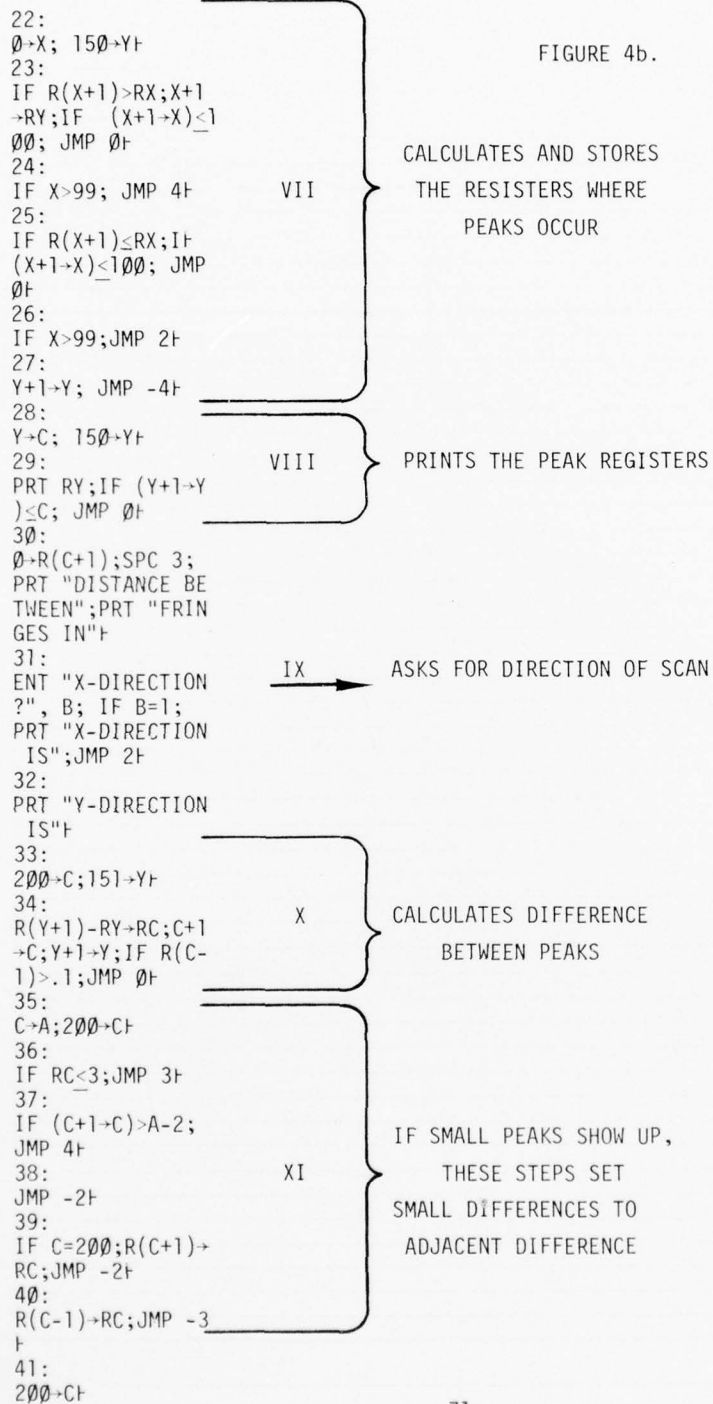
A good method of examining the procedure used to count the fringes would be to look at Figure 4a, b, and c, which list the calculator program, in some detail.

The first step is to image the fringe pattern onto the scanning aperture plane and position the aperture in the y direction ready to scan across the complete fringe pattern.

By simultaneously running the program and starting the y direction scan (manually), the "reads data" portion of the program begins reading in the fringe information to the designated registers R0 - through R100. Following the 25 second data read in time, the program initializes step II which normalizes the data such that the minimum voltage register is zero and all other registers are shifted about the zero level. Section III in the program finds the register with maximum value and affixes this value to the scale setting needed for plotting the 100 data registers (IV) representing the fringe pattern. The fifth portion points out the data

FIGURE 4a.





AFAL-TR-77-203

<pre> 42: RC+R (C+1)→R(C-1) ↑ 43: C+1→C; IF C≤A-3; JMP -1↑ 44: IF B=1; JMP 2↑ 45: Ø→R25Ø; FXD 3; PRT .Ø18(R(A-2)/ (A-2Ø1))→R25Ø; PRT" INCHES"; SPC 8; JMP 2↑ 46: Ø→R251; FXD 3; PRT .Ø29(R(A-2)/ (A-2Ø1))→R251; PRT" INCHES"; SPC 8↑ 47: STP ↑ 48: PRT "DISTANCE BE TWEEN"; PRT "FRIN GES IS"↑ 49: PRT R251/Γ(1+R25 1R251/R25ØR25Ø)→ R252↑ 5Ø: PRT" INCHES"; SPC 1; PRT "AN GLE WITH"; PRT "R ESPECT TO"; PRT" THE X-AXIS"↑ 51: PRT ACS (R252/R2 51); PRT" DEGREES"; SPC 8↑ 52: END ↑ R276 </pre>	<div style="display: flex; align-items: center; justify-content: center;"> <div style="font-size: 3em; margin-right: 10px;">}</div> <div style="text-align: center;"> <p>XII</p> </div> <div style="margin-left: 10px;"> <p>CALCULATES SUM OF PEAK DIFFERENCES AND STORES</p> </div> </div> <div style="display: flex; align-items: center; justify-content: center; margin-top: 20px;"> <div style="font-size: 3em; margin-right: 10px;">}</div> <div style="text-align: center;"> <p>XIII</p> </div> <div style="margin-left: 10px;"> <p>CALCULATES AND PRINTS FRINGE SPACING IN BOTH THE X & Y DIRECTION</p> </div> </div> <div style="display: flex; align-items: center; justify-content: center; margin-top: 20px;"> <div style="font-size: 3em; margin-right: 10px;">}</div> <div style="text-align: center;"> <p>XIV</p> </div> <div style="margin-left: 10px;"> <p>FROM X & Y FRINGE SPACING THE ACTUAL FRINGE SPACING AND DIRECTION ARE PRINTED IN INCHES AND DEGREES, RESPECTIVELY</p> </div> </div>
--	---

FIGURE 4c.

AD-A048 210

AIR FORCE AVIONICS LAB WRIGHT-PATTERSON AFB OHIO
SPECKLEGRAM DATA REDUCTION USING OPTICAL AND DIGITAL TECHNIQUES--ETC(U)
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2 OF 2

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registers that contain fringe data or, in other words, registers with data more than 5×10^{-2} in amplitude. This information merely tells the programmer if noise contained in the systems will be above a certain threshold value set by the programmer (5×10^{-2} in this case), and immediately following is Section VI which sets these noise values to absolute zero. The plots and printouts in Sections III, IV, AND V are mainly used to check the program for proper operation and are normally eliminated for general purposes by the jump 9 command in statement 9 of Section III. The first printout under normal operation, performed in Section VII, calculates the registers where the peaks of the fringes occur by a method of adjacent register comparison, and a resulting printout is executed in Section VIII. An example of this printout is shown in Figures 5a and 5b. These fringes will be discussed in more detail later in the report. Section IX of the computer program simply asks the operator the direction in which the data was scanned in from Section I, and correspondingly enters a scale factor that has been manually precalculated to convert the scanning motor speeds into a recognizable format such as inches for this case. These two scale factors show up in Section XIII of the program as .018 for the y-direction and .029 for the x-direction. In Section X the data stored in Section VII are subtracted and these differences are stored again for later use in Sections XI and XII. The eleventh program section is a safety feature installed to ensure that any peaks appearing as a result of noise in the system that were not eliminated previously are thrown out to prevent a false representation of fringe count. The fringe differences are now averaged over the entire data file in Section XII and the uni-directional (y) spacing is calculated with the motor speed scale factor employed to give an answer in inches. After storing this spacing in inches the entire procedure is initiated again the x-direction, by scanning the motor drive and this time using a different scale factor. As a result of Section XIII both x and y fringe spacing information is stored in R251 and R250, respectively. Stepping to the final section (XIV) registers R250 and R251 containing the x and y information, are inserted into a simple trigonometry function to determine the fringe spacing d and fringe angle θ which are the two answers being sought (see Figure 4D).

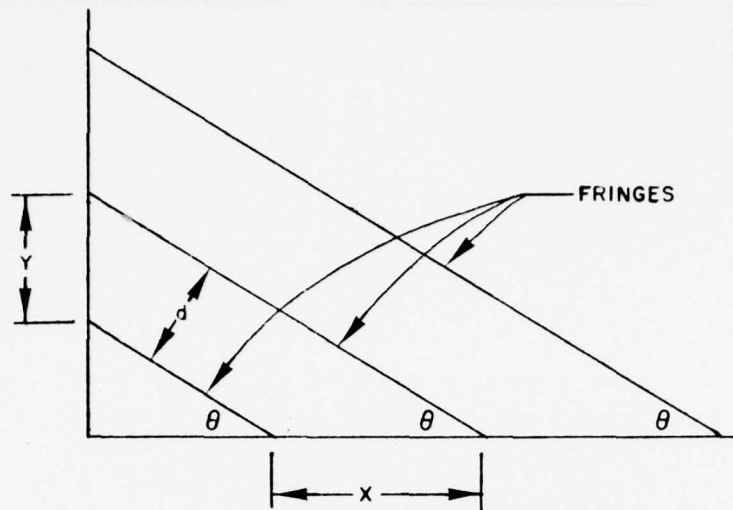


Figure 4D

Figures 5a and 5b illustrate the format in which the results were displayed. The answers of 5a were made from fringes spaced at .05 inch apart and 5b .10 inch apart, with angles for the two sets of fringes set approximately the same.

Finally 6 illustrates a method for checking the fringe angles, by simply plotting the fringe pattern in the x and y direction and graphically measuring the angle offset.

THE PEAKS ARE
AT REGISTERS

χ

0
13
17
21
26
30
35
39

DISTANCE BETWEEN
FRINGES IN
X-DIRECTION IS

.126
INCHES

DISTANCE BETWEEN
FRINGES IS

.099
INCHES

THE PEAKS ARE
AT REGISTERS

y

0
49
57
67
76

ANGLE WITH
RESPECT TO
THE X-AXIS

37.001
DEGREES

DISTANCE BETWEEN
FRINGES IN
Y-DIRECTION IS

.162
INCHES

Figure 5a

THE PEAKS ARE
AT REGISTERS

y
0
43
47
51
55
59
64
68
73

DISTANCE BETWEEN
FRINGES IN
Y-DIRECTION IS

.077

INCHES

DISTANCE BETWEEN
FRINGES IS

.050

INCHES

THE PEAKS ARE
AT REGISTERS

x
0
14
17
19
21
23
26
28
30
32
35
37
39

ANGLE WITH
RESPECT TO
THE X-AXIS

40.510

DEGREES

DISTANCE BETWEEN
FRINGES IN
X-DIRECTION IS

.066

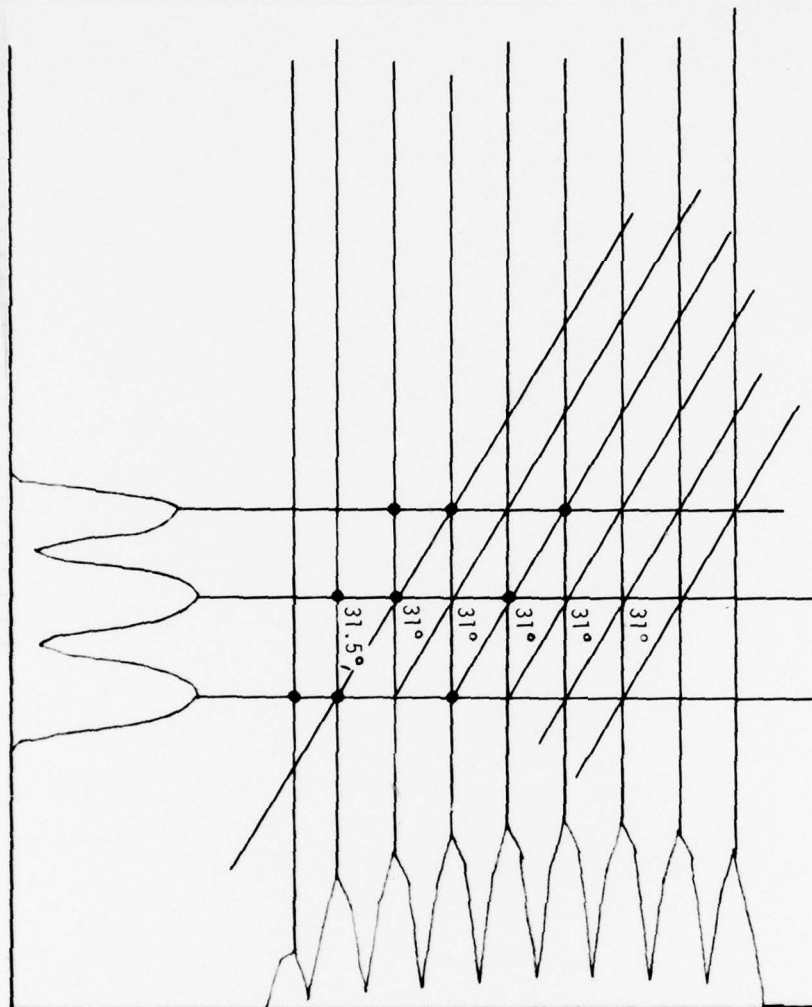
INCHES

Figure 5b


```

0:
0-X;AXE 0,0,0,0+
1:
RED 3,A,RX;IF (X
+1-X)≤100;JMP 0+
2:
0-X;SCL 0,100,0,
1+
3:
PLT 1.45X,RX;IF
(X+1-X)≤100;JMP
0+
4:
STP +
5:
0-X+
6:
RED 3,A,RX;IF (X
+1-X)≤100;JMP 0+
7:
0-X;SCL 0,1,0,10
0+
8:
PLT RX,.9X;IF (X
+1-X)≤100;JMP 0+
9:
END +
R395

```



THE PEAKS ARE
AT REGISTERS
0.00000000E 00
1.40000000E 01
2.60000000E 01
3.60000000E 01

DISTANCE BETWEEN
FRINGES IS
.216
INCHES

THE PEAKS ARE
AT REGISTERS
0.000
7.000
11.000
15.000
19.000
23.000
27.000
31.000
35.000
39.000

DISTANCE BETWEEN
FRINGES IS
.116
INCHES
DISTANCE BETWEEN
FRINGES IS
.102

ANGLE WITH
RESPECT TO
THE X-AXIS
28.237

Figure 6

CONCLUSION:

Our investigation as described here, indicates that several techniques may readily be applied to the type of fringe counting problem considered.

Several choices exist for reading out and for processing ("counting") fringe spacing. The choices of techniques (and optimum hardware implementation of same) depend heavily on the detailed technical and economic parameters and constraints of the application. Consideration of these details was beyond the scope of these initial feasibility investigations, since all equipment used in the demonstrations was presently available in-house.

The next logical step appears to be a design analysis to determine the optimum system configuration taking into account the detailed technical and economic factors. Following this, construction and testing of a prototype system would be appropriate.

AFAL/TEL would be pleased to undertake further work on this problem along the lines of the previous paragraph or as considered appropriate by mutual agreement of AFAL and FDL.

APPENDIX II

CONTROL PROGRAM PRINTOUT

SPECKLEGRAM ANALYSIS SYSTEM

MACRO VP05-01H 05-NOV-72 02:24 PAGE 1

.TITLE SPECKLEGRAM ANALYSIS SYSTEM
:WITH DATA READ FROM RETICON
:AND STEPPING STAGE

.ENABLE AMA

R0=%0
R1=%1
R2=%2
R3=%3
R4=%4
P5=%5
SP=%6
PC=%7
KBS=177560
KBB=177562
TPS=177564
TPB=177566

.ASECT

:MAIN PROGRAM

```

000500 012766 000500
000500 005037 005742
000510 012700 006062
000514 004737 004210
000520 012700 005762
000524 004737 004320
000530 012700 005762
000534 012702 005666
000540 004737 001034
000544 010337 005744
000550 012737 000005
000556 012700 005776
000562 005020
000564 020027 006056
000570 001374
000572 012700 000144
000576 004737 004210
000602 012700 005776
000606 004737 004320
000612 012700 005776

```

JUMP: MOV #XLINIT,R0
CLEAR: CLP (R0)+
CMP R0,#STEPX
BNE CLEAR
MOV #XDIST,R0
JSR PC,TTYOUT
MOV #XLINIT,R0
JSR PC,INPUT
MOV #XLINIT,R0

:PRINT AVERAGE
:ENTER NUMBER
:CONVERT TO OCTAL
:LOAD
:X
:CLEAR STAGING LOCATIONS
:PRINT X-DISTANCE
:ENTER X-DISTANCE

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SPECKLEGRAM ANALYSIS SYSTEM

MACRO VR05-01H 05-NOV-72 02:24 PAGE 1+

48 000616	012702	005666	MOV #KEEP,R2		
49 000622	004737	001034	JSR PC,ASCII		:CONVT TO OCTAL
50 000626	012700	005776	MOV #XLIMIT,R0		:LOAD
51 000632	010310		MOV R3,(R0)		
52 000634	012700	006234	MOV #YDIST,R0		:PRINT "Y-DISTANCE"
53 000640	004737	004210	JSR PC,TTYOUT		:ENTER Y-DISTANCE
54 000644	012700	006012	MOV #YLIMIT,R0		
55 000650	004737	004320	JSR PC,INPUT		
56 000654	012700	006012	MOV #YLIMIT,R0		:CNVT TO OCTAL
57 000660	012702	005666	MOV #KEEP,R2		
58 000664	004737	001034	JSR PC,ASCII		:PRINT "X-INC"
59 000670	010337	006012	MOV R3,YLIMIT		:ENTER X-INC
60 000674	012700	006324	MOV #XINC,R0		PRINT "Y-INC"
61 000700	004737	004210	JSR PC,TTYOUT		ENTER Y-INC
62 000704	012700	006026	MOV #INCX,R0		SET, +DIRECTION
63 000710	004737	004320	JSR PC,INPUT		
64 000714	012700	006374	MOV #YINC,R0		:X-INC TO OCTAL
65 000720	004737	004210	JSR PC,TTYOUT		LOAD
66 000724	012700	006042	MOV #INCY,R0		Y-STEP TO OCTAL
67 000730	004737	004320	JSR PC,INPUT		PRINT HEADER
68 000734	012737	000004	MOV #4,0*164002:		GTO STAGE ROUTINE
69 000742	012700	006026	MOV #INCX,R0		PRINT "SCAN COMPLETE"
70 000746	012702	005666	MOV #KEEP,R2		
71 000752	004737	001034	JSR PC,ASCII		
72 000756	013737	005644	MOV #BUF,STEPX:		
73 000764	012700	006042	MOV #INCY,R0		
74 000770	012702	005666	MOV #KEEP,R2		
75 000774	004737	001034	JSR PC,ASCII		
76 001000	012700	006576	MOV #HEAD,R0:		
77 001004	004737	004210	JSR PC,TTYOUT		
78 001010	013737	005044	MOV #BUF,STEPY		
79 001016	004737	005132	JSR PC,ASTAGE:		
80 001022	012700	006450	MOV #FIN,R0		
81 001026	004737	004210	JSR PC,TTYOUT:		
82 001032	000000		HALT		
83					
84					
85					
86 001034	012001		ASCII: MOV (R0)+,R1:		CONVERT ASCII TO OCTAL
87 001036	162701	000060	SUB #60,R1		
88 001042	010122		MOV R1,(R2)+		
89 001044	021027	000015	CMP (R0),#15		
90 001050	001371		BNE ASCII		
91 001052	005003		CLR R3		
92 001054	014203		MOV ~(R2),R3:		LOAD LSD
93 001056	020227	005666	CMP R2,#KEEP		
94 001062	001465		BEO CMS		

SPECKLEGRAM ANALYSIS SYSTEM

MACRO VP05-01H 05-NOV-72 02:24 PAGE 1+

95 001054	014205	MOV -(R2),R5;	LOAD 2ND DIGIT
96 001066	005004	CLR R4	
97 001070	020527	CMP R5,#0	
98 001074	001405	BEQ .+14	
99 001076	062704	ADD #12,R4;	10.
100 001102	162705	SUB #1,R5	
101 001106	000770	BR .-16	
102 001110	060403	ADD R4,R3	
103 001112	020227	CMP R2,*KEEP	
104 001116	001447	BEQ CNST	
105 001120	014205	MOV -(R2),R5;	LOAD 3RD DIGIT
106 001122	005004	CLR R4	
107 001124	020527	CMP R5,#0	
108 001130	001405	BEQ .+14	
109 001132	062704	ADD #144,R4;	100.
110 001136	162705	SUB #1,R5	
111 001142	000770	BR .-16	
112 001144	060403	ADD R4,R3	
113 001146	020227	CMP R2,*KEEP	
114 001152	001431	BEQ CNST	
115 001154	014205	MOV -(R2),R5;	LOAD 5TH DIGIT
116 001156	005004	CLR R4	
117 001160	020527	CMP R5,#0	
118 001164	001405	BEQ .+14	
119 001166	062704	ADD #1750,R4;	1000.
120 001172	162705	SUB #1,R5	
121 001176	000770	BR .-16	
122 001200	060403	ADD R4,R3	
123 001202	020227	CMP R2,*KEEP	
124 001205	001413	BEQ CNST	
125 001210	014205	MOV -(R2),R5;	LOAD 5TH DIGIT
126 001212	005004	CLR R4	
127 001214	020527	CMP R5,#0	
128 001220	001405	BEQ .+14	
129 001222	062704	ADD #23420,R4;	10000.
130 001226	162705	SUB #1,R5	
131 001232	000770	BR .-16	
132 001234	060403	ADD R4,R3	
133 001236	012701	MOV #0BUF,R1;	LOAD FINAL TO 0BUF
134 001242	010311	MOV R3,(R1)	
135 001244	000207	RTS PC	
136			
137			
138 001246	000000	AMANIP:HALT	
139 001250	012700	MANIP: MOV #RRD,R0	
140 001254	005020	CLR (R0)+;	CLEAR WORKING REGISTERS
141 001256	020027	CMP R0,*0BUF+2;	PLUS NONE,0BUF,FUNC

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SPECKLEGRAM ANALYSIS SYSTEM

MACRO VR05-01H 05-NOV-72 02:24 PAGE 1+

142 001262	001374		BNE CLR1:	KEEP,FLG
143 001264	012700	007022	MOV #FBUFFAV,R0	
144 001270	005020		CLR (R0)+:	CLEAR FFT BUFFERS
145 001272	020027	010044	CMP R0,#FFTBUFF+410	
146 001276	001374		BNE CLR2	
147 001300	012704	007434	MOV #FFTBUFF,R4	GTO READ ROUTINE
148 001304	004737	003216	JSR PC,AREAD:	GTO FFT ROUTINE
149 001310	004737	001462	JSR PC,AFRT:	GTO AMPLITUDE ROUTINE
150 001314	004737	004076	JSR PC,ANIP:	GTO FREQUENCY ROUTINE
151 001320	004737	004516	JSR PC,AFREQ:	
152 001324	012700	006742	MOV #SPC,R0	INSERT SPACES
153 001330	004737	004210	JSR PC,TTYOUT:	
154 001334	023727	005642	CMP NONE,#1	
155 001342	001005		BNE HUIPS	
156 001344	012700	006444	MOV #GOOD,R0	PRINT "LOW
157 001350	004737	004210	JSR PC,TTYOUT:	
158 001354	000410		BR NOLIST	
159 001356	013700	005644	HUMPS: MOV OBUFF,R0	FREQUENCY TO DECIMAL
160 001362	004737	004754	JSR PC,OTD:	
161 001366	012700	005704	MOV #DBUFF+2,R0	PRINT FREQUENCY
162 001372	004737	004210	JSR PC,TTYOUT:	
163 001376	005237	005746	NOLIST: INC RATHER	
164 001402	013727	005644	MOV OBUFF,ROBUF	
165 001410	013737	005646	MOV OBUFF+2,ROBUF+2	
166 001416	023727	005746	CMP RATHER,#2	
167 001424	001310		BNE ANHHP	
168 001426	012700	006742	MOV #SPC,R0	
169 001432	004737	004210	JSR PC,TTYOUT	
170 001436	004737	003640	JSR PC,APRINT	
171 001442	012700	006756	MOV #EOL,R0	
172 001446	004737	004210	JSR PC,TTYOUT:	LF , CR
173 001452	000207		RTS PC	
174 001454	000137	000500	JMP START	
175 001460	000000		HALT	
176				
177				
178 001462	000000		AFRT: HALT	FFT SUBROUTINE
179 001464	012700	007434	MOV #FFTBUFF,R0:	
180 001470	012701	007436	MOV #FFTBUFF+2,R1	
181 001474	022120		NORMAL: CMP (R1)+,(R0)+	
182 001476	100001		BPL STORE	
183 001500	000775		BR NORMAL	
184 001502	162701	000002	STORE: SUB #2,R1	
185 001506	012103		ADD: MOV (R1)+,R3	
186 001510	021103		BDO: CMP (R1),R3	
187 001512	100375		BPL ADD	
188 001514	062701	000002	ADD #2,R1	

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SPECKLEGRAM ANALYSIS SYSTEM

MACRO VR05-01H 05-NOV-72 02:24 PAGE 1+

189 001520	020127	007644	CHP R1.#FFTBUF+210
190 001524	001371		BNE B00
191 001526	020337	001000	CHP R3.#1000
192 001532	001425		SEQ C10
193 001534	003016		SGT DROP
194 001536	020327	000400	CHP R3.#400
195 001542	003021		SGT C10
196 001544	006303		SEE: ASL R3
197 001546	012700	007434	MOV #FFTBUF,R0
198 001552	006320		ASL (R0)+
199 001554	020027	007644	UP: CHP R0.#FFTBUF+210
200 001560	001374		BNE UP
201 001562	020327	000400	CHP R3.#400
202 001566	003766		BLE SEE
203 001570	000406		BR C10
204 001572	012700	007434	DROP: MOV #FFTBUF,R0
205 001576	006220		DOWN: ASR (R0)+
206 001600	020027	007644	CHP R0.#FFTBUF+210
207 001604	001374		BNE DOWN
208 001606	012700	007434	CDO: MOV #FFTBUF,R0
209 001612	012701	007444	MOV #FFTBUF+10,R1
210 001616	012120		SLIP: MOV (R1)+(R0)+
211 001620	020027	007654	CHP R0.#FFTBUF+220
212 001624	001374		BNE SLIP
213 001626	012737	000002	MOV #2,RR9
214 001634	012737	000001	MOV #1,RR0
215 001642	012737	000200	MOV #200,RR2
216 001650	005700		TST R0
217 001652	005001		CLR R1
218 001654	012700	007434	MOV #FFTBUF,R0
219 001660	006210		SHIFT: ASR (R0)
220 001662	005201		INC R1
221 001664	020127	000003	CHP R1.#3
222 001670	001373		BNE SHIFT
223 001672	005001		CLR R1
224 001674	062700	000002	A10 #2,R0
225 001700	020027	010036	CHP R0.#FFTBUF+402
226 001704	001365		BNE SHIFT
227 001706	005700		ALPHA: TST R0
228 001710	012704	007434	MOV #FFTBUF,R4
229 001714	006224		KILL: ASR (R4)+
230 001716	020427	010034	CHP R4.#FFTBUF+400
231 001722	001374		BNE KILL
232 001724	012737	000000	MOV #0,RR1
233 001732	006237	005610	ASR RR2
234 001736	005700		BETA: TST R0
235 001740	012704	010674	MOV #COS,R4

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SPECKLEGRAM ANALYSIS SYSTEM

MACRO YR05-01H 05-NOV-72 02:24 PAGE 1+

236 001744	063704	005624	ADD R08,R4
237 001750	011437	005612	MOV (R4),R03
238 001754	012704	011000	MOV #01H,R4
239 001760	063704	005624	ADD R08,R4
240 001764	011437	005614	MOV (R4),R04
241 001770	013737	005606	MOV R01,R05
242 001776	005700		TST R0
243 002000	013700	005616	MOV R05,R0
244 002004	062700	007434	ADD #FF00H,R0 :3000
245 002010	010037	005620	MOV R0,R06
246 002014	013701	005610	MOV R02,R1
247 002020	060001		ADD R0,R1
248 002022	010137	005622	MOV R1,R07
249 002026	017700	003566	MOV R006,R0
250 002032	017701	003564	MOV R007,R1
251 002036	060001		ADD R0,R1
252 002040	010137	005632	MOV R1,B
253 002044	013700	005620	MOV R06,R0
254 002050	062700	000200	ADD #200,R0
255 002054	013701	005622	MOV R07,R1
256 002060	062701	000200	ADD #200,R1
257 002064	011102		MOV (R1),R2
258 002066	061002	005634	ADD (R0),R2
259 002070	010237	005620	MOV R2,C
260 002074	013700		MOV R06,R0
261 002100	011004		MOV (R0),R4
262 002102	013701	005622	MOV R07,R1
263 002106	161104		SUB (R1),R4
264 002110	005005		CLR R5
265 002112	013702	005612	MOV R03,R2
266 002116	005704		TST R4
267 002120	100005		BPL OTHER
268 002122	005702		TST R2
269 002124	100020		BPL MINUS
270 002126	005404		NEG R4
271 002130	005402		NEG R2
272 002132	000404		BR PLUS
273 002134	005702		TST R2
274 002136	100002		BPL PLUS
275 002140	005402		NEG R2
276 002142	000411		BR MINUS
277 002144	032704		BIT #1,R4
278 002150	001401	000001	DEO AZERO
279 002152	060205		ADD R2,R5
280 002154	006302		ASL R2
281 002156	006204		ASR R4
282 002160	001371		BNE PLUS

SPECKLEGRAM ANALYSIS SYSTEM

MACRO VR05-Q1H 05-NOV-72 02:24 PAGE 1+

283 002162 005004 CLR R4
 284 002164 000407 BR LOAD
 285 002166 005704 MINUS: TST R4
 286 002170 100001 BPL GOON
 287 002172 005404 NEG R4
 288 002174 012737 000001 005664 GOON: MOV #1.FLG
 289 002202 000760 BR PLUS
 290 002204 005705 TST R5
 291 002206 100002 LOAD: BPL FUD1
 292 002210 012705 077777 FUD1: MOV #77777.R5
 293 002214 006205 ASR R5
 294 002216 005204 INC R4
 295 002220 020427 000011 CIP R4.#11
 296 002224 001373 DNE FUD1
 297 002226 023727 005664 000001 CIP FLG.#1
 298 002234 001004 DNE JUG
 299 002236 005405 NEG R5
 300 002240 012737 000000 005664 JUG: MOV #0.FLG
 301 002246 062700 000200 ADD #200.R0
 302 002252 062701 000200 ADD #200.R1
 303 002256 011102 MOV (R1).R2
 304 002260 161002 SUB (R0).R2
 305 002262 013704 005614 MOV RR4.R4
 306 002266 005003 CLR R3
 307 002270 005702 TST R2
 308 002272 100004 BPL AG1
 309 002274 005402 NEG R2
 310 002276 012737 000001 005664 AG1: MOV #1.FLG
 311 002304 032702 000001 BIT #1.R2
 312 002310 001401 BEQ BZERO
 313 002312 060403 ADD R4.R3
 314 002314 005304 ASL R4
 315 002316 006202 ASR R2
 316 002320 001371 DNE AG1
 317 002322 005004 CLR R4
 318 002324 005703 AG2: TST R3
 319 002326 100002 BPL FUD2
 320 002330 012703 077777 FUD2: MOV #77777.R3
 321 002334 006203 ASR R3
 322 002336 005204 INC R4
 323 002340 020427 CIP R4.#11
 324 002344 001373 DNE FUD2
 325 002346 023727 005664 000001 CIP FLG.#1
 326 002354 001004 DNE AG3
 327 002356 012737 000000 005664 MOV #0.FLG
 328 002364 005403 NEG R3
 329 002366 060305 AG3: ADD R3.R5

PECKLEGRAH ANALYSIS SYSTEM

MACRO VR05-01H 05-NOV-72 02:24 PAGE 1+

320 002370	010537	005630	MOV R5,R
331 002374	013700	005620	MOV R6,R0
332 002400	01004		MOV (R0),R4
333 002402	013701	005622	MOV R7,R1
334 002406	161104		SUB (R1),R4
335 002410	005005		CLR R5
336 002412	013702	005614	MOV R4,R2
337 002416	005704		TST R4
338 002420	100004		BPL MULT4
339 002422	005404		NEG R4
340 002424	012737	000001 005664	MOV #1,FLG
341 002432	032704		BIT #1,R4
342 002436	001401		BEQ DZERO
343 002440	060205		ADD R2,R5
344 002442	006302		ASL R2
345 002444	006204		ASR R4
346 002446	001371		BNE MULT4
347 002450	005004		CLR R4
348 002452	000400		BR CHECK
349 002454	005705		CHECK: TST R5
350 002456	100002		BPL FUD3
351 002460	012705	077777	MOV #7777,R5
352 002464	006205		ASR R5
353 002466	005204		INC R4
354 002470	020427	000011	CHP R4,#11
355 002474	001373		BNE FUD3
356 002476	023727	005664 000001	CHP FLG,#1
357 002504	001004		BNE EAT
358 002506	012737	000000 005664	MOV #0,FLG
359 002514	005405		NEG R5
360 002516	062700		ADD #200,R0
361 002522	011002		MOV (R0),R2
362 002524	062701	000200	ADD #200,R1
363 002530	161102		SUB (R1),R2
364 002532	013703	005612	MOV R3,R3
365 002536	005004		CLR R4
366 002540	005703		TST R3
367 002542	100005		BPL DOT
368 002544	005702		TST P2
369 002546	100020		BPL LOW
370 002550	005402		NEG R2
371 002552	005403		NEG R3
372 002554	000404		BR HIGH
373 002556	005702		TST R2
374 002560	100002		BPL HIGH
375 002562	005402		NEG R2
376 002564	000411		BR LOW

SPECKLEGRAM ANALYSIS SYSTEM

MCPRO VR05-01H 05-NOV-72 02:24 PAGE 1+

```

377 002566 032702 000001 HIGH: BIT #1,R2
378 002572 001401 0E0 CZERO
379 002574 060304 ADD R3,R4
380 002576 006303 CZERO: ASL R3
381 002600 00C202 ASR R2
382 002602 001371 BNE HIGH
383 002604 005003 CLR R3
384 002606 000407 ER ALOAD
385 002610 005703 TST R3
386 002612 100001 EPL GOONY
387 002614 005403 NEG R3
388 002616 012737 GOONY: MOV #1,FLG
389 002624 000700 ER HIGH
390 002626 005704 ALOAD: TST R4
391 002630 100002 EPL FUD4
392 002632 012704 MOV #7777,R4
393 002636 006204 FUD4: ASR R4
394 002640 005203 INR R3
395 002642 020327 CMP R3,#11
396 002646 001373 BNE FUD4
397 002650 023727 CMP FLG,#1
398 002656 001004 BNE JUGGER
399 002660 005404 NEG R4
400 002662 012737 JUGGER:ADD R4,R5
401 002670 060405 MOV R5,(R1)
402 002672 010511 L8.: MOV B,0RR6
403 002674 013777 MOV R6,R0
404 002702 013700 ADD #200,R0
405 002706 062700 MOV C,(R0)
406 002712 013710 MOV A,0RR7
407 002716 013777 MOV R5,R5
408 002724 013705 MOV R2,R2
409 002730 013702 MOV R2,R0
410 002734 010200 TST R0
411 002736 060200 TST R0
412 002740 005700 ADD R0,R5
413 002742 005700 MOV R5,R5
414 002744 060005 L10.: ADD R2,R5
415 002746 010537 CMP R5,#177:
416 002752 060205 BGT L11.
417 002754 020527 JMP GAMA
418 002760 003002 ADD #2,RR1
419 002762 000137 CMP RR2,RR1
420 002766 062737 BEO L12.
421 002774 023737 ADD RR9,RR8
422 003002 001405
423 003004 063737

```

:JUGGLE FFT DATA

SPECKLEGRAM ANALYSIS SYSTEM

MACRO VR05-01H 05-NOV-72 02:24 PAGE 1+

```

24 003012 000137 001736 JNP BETA
25 003016 062737 000001 ADD #1,RR0
126 003024 023727 005604 CMP RR0,#6
427 003032 003007 000006 BGT D
428 003034 006337 005626 ACL RR9
429 003040 012737 000000 MOV #0,RR8
430 003046 000137 001706 JNP ALPHA
431 003052 012737 000001 D:
432 003060 012737 000001 BEGIN:
433 003066 012737 000040 MOV #1,RR2:
434 003074 005004 MOV #1,RR0
435 003076 013702 005610 MOV #40,RR1
436 003102 013700 005604 CLR R4
437 003106 013701 005606 MOV RR2,R2
438 003112 030102 MOV RR0,R0
439 003114 001401 MOV RR1,R1
440 003116 060004 TEST: BIT R1,R2
441 003120 006201 BEO SLIDE
442 003122 006300 MOV R0,R4
443 003124 020127 ASL R1
444 003130 001370 ASL R0
445 003132 020402 CMP R1,#0
446 003134 002430 BNE TEST
447 003136 006302 CMP R4,R2
448 003140 006304 BLT RECLR
449 003142 062702 ASL R2
450 003146 062704 ASL R4
451 003152 011203 ADD #FFTBUFF,R2
452 003154 011412 ADD #FFTBUFF,R4
453 003156 010314 MOV (R2),R3
454 003160 062702 MOV (R4),(R2)
455 003164 062704 MOV R3,(R4)
456 003170 011203 ADD #200,R2
457 003172 011412 ADD #200,R4
458 003174 010314 MOV (R2),R3
459 003176 062737 MOV (R4),(R2)
460 003204 023727 MOV R3,(R4)
461 003212 001322 RECLR: ADD #1,RR2
462 003214 000207 CMP RR2,#100
463 464 BNE BEGIN
465 466 RTS PC
467
468 003216 000000 AREAD: HALT
469 003220 005002 READ: CLR R2:
470 003222 005005 CLR R5

```

READ DATA FROM RETICON

AREAD: HALT
READ: CLR R2:
CLR R5

SPECKLEGRAM ANALYSIS SYSTEM

MACRO VR05-01H 05-NOV-72 02:24 PAGE 1+

```

471 003224 012737 000004 164000 176770
472 003232 012737 001005 176770
473 003240 013700 176770
474 003244 122700 000177
475 003250 100373 176772
476 003252 013701 000377
477 003256 020127 000002
478 003262 100360
479 003264 020527
480 003270 001402
481 003272 005305
482 003274 000753
483 003276 005003
484 003300 012737 000004 164000
485 003306 005202
486 003310 020227
487 003314 001405
488 003316 005303
489 003320 020327
490 003324 001374
491 003326 000763
492 003330 005237
493 003334 023737 005744
494 003342 003035
495 003344 012737
496 003352 013737
497 003360 013705
498 003364 122705
499 003370 100373
500 003372 013724
501 003376 005700
502 003400 005700
503 003402 005700
504 003404 005700
505 003406 073727
506 003414 001004
507 003416 020427
508 003422 001350
509 003424 000434
510 003426 020427
511 003432 001344
512 003434 000430
513 003436 012737
514 003444 012737
515 003452 013705
516 003456 122705
517 003462 100373

CLOCK PULSE
CHANNEL 2
DONE READING ?
LOAD A/D
DO I HAVE DATA ?
DELAY
WAIT: CLR R3
CLOCK2: MOV #4, R164000;
INC R2
CMP R2, #202;
BEO CLOCK3
SLOW: INC R3;
CMP R3, #5;
BNE SLOW
BR WAIT
CLOCK3: INC SECOND;
CMP SECOND, TIMES
BGT CLOCK5
CLOCK4: MOV #4, R164000;
MOV XREAD, R176770
DONE2: MOV R176770, R5
CMPB #177, R5;
BPL DONE2
AVER: MOV R176772, (R4)+;
TST R0
TST R0
TST R0
CIP WHICH, #1;
BNE LOOP1
CIP R4, #FFBFAV+210;
BNE CLOCK4
BR INPREAD
LOOP1: CIP R4, #FFTBUFF+210;
BNE CLOCK4
BR INPREAD
CLOCK5: MOV #4, R164000;
MOV #405, R176770
DONE3: MOV R176770, R5
CMPB #177, R5
BPL DONE3

XREAD OR YREAD
CLOCK PULSE-X
: DONE ?
LOAD A/D
: AVERAGE
AVERAGE -X
CLOCK PULSE-Y

```

SPECKLEGRAM ANALYSIS SYSTEM

MACRO VR05-01H 05-NOV-72 02:24 PAGE 1+

```

518 003464 013724 176772      MOV @*176772,(R4)+
519 003470 023727 005740 000001  CMP WHICH,*1
520 003476 001004      BNE LOOP2
521 003500 020427 007232      CMP R4,#FBUF+210
522 003504 001354      BNE CLOCKS
523 003506 000403      BR DIFREAD
524 003510 020427 007644      LOOP2:  CMP R4,#FFTBUFF+210
525 003514 001350      BNE CLOCKS
526 003516 005237 005742      DNREAD: INC TRACK
527 003522 023737 005742 005744  CMP TRACK,TIMES
528 003530 001424      BEQ FOWARD
529 003532 023727 005742 000001  CMP TRACK,*1
530 003540 001412      BEQ DUPRED
531 003542 012702 007434      MOV #FFTBUFF,R2
532 003546 012705 007022      MOV #FBUFFAV,R5
533 003552 006212      ALOOP:  ASR (R2)
534 003554 006215      ASR (R5)
535 003556 062522      ADD (R5)+,(R2)+
536 003560 020227 007644      CMP R2,#FFTBUFF+210
537 003564 001372      BNE ALOOP
538 003566 012737 000001 005740  DUPRED: MOV #1,WHICH
539 003574 012704 007022      MOV #FBUFFAV,R4
540 003600 000606      BR AHEAD
541 003602 005037 005742      FOWARD: CLR TRACK
542 003606 005037 005740      CLR WHICH
543 003612 012700 007444      MOV #FFTBUFF+10,R0:
544 003616 012701 007644      MOV #FFTBUFF+210,R1
545 003622 011120      CIRCLE:MOV (R1),(R0)+
546 003624 162701 000002      SUB #2,R1
547 003630 020027 007544      CMP R0,#FFTBUFF+110
548 003634 001372      BNE CIRCLE
549 003636 000207      RTS PC
550
551
552
553
554
555 003640 000000      APRINT:HALT
556 003642 005037 005752      PRINT:  CLR YD1ST0
557 003646 005037 005750      CLR XD1ST0
558 003652 012705 000100      MOV #100,R5
559 003656 163705 005756      SUB ROBUFF,R5
560 003662 005237 005750      INC XD1ST0
561 003666 020527 000000      CMP RS,#0
562 003672 003371      BGT ,-14
563 003674 012705 000100      MOV #100,R5
564 003700 163705 005644      SUB OBUFF,R5

```

LOAD 1ST HALF DATA TO 2ND HALF

SPECKLEGRAM ANALYSIS SYSTEM

MACRO VR05-01H 05-NOV-72 02:24 PAGE 1+

```

565 003704 005237 005752      INC YDISTO
566 003710 020527 000000      CMP R5,*0
567 003714 003371              BGT ,-14
568 003716 004737 003760      JSR PC,ANGLE:
569 003722 012700 005706      MOV #DBUF+4,R0:
570 003726 004737 004210      JSR PC,TTYOUT
571 003732 012700 006742      MOV #SPC,R0
572 003736 004737 004210      JSR PC,TTYOUT:
573 003742 004737 004424      JSR PC,ADISP
574 003746 012700 005706      MOV #DBUF+4,R0,
575 003752 004737 004210      JSR PC,TTYOUT
576 003756 000207      RTS PC
577
578
579
580
581 003760 000000      ANGLE:HALT
582 003762 005000      ANGLE: CLR R0
583 003764 013703 005752      MOV YDISTO,R3:
584 003770 013704 005750      MOV XDISTO,R4:
585 003774 006303      MULTI: ASL R3:
586 003776 005200      INC R0
587 004000 020027      CMP R0,*6
588 004004 001373      BNC MULTI
589 004006 005000      CLR R0
590 004010 160403      DOCIR: SUB R4,R3 :
591 004012 062700 000001      ADD #1,R0
592 004016 020327 000000      CMP R3,*0
593 004022 001372      DNE DOCIR
594 004024 012705 010134      MOV #TANBUF,R5:
595 004030 020025      LOOKUP: CMP R0,(R5)+:
596 004032 100376      BPL LOOKUP
597 004034 162705 000004      SUB #4,R5
598 004040 162705 010134      SUB #TANBUF,R5:
599 004044 010537 005754      MOV R5,RAT10:
600 004050 006205      DIVANG: ASR R5:
601 004052 012704 005702      MOV #DBUF,R4
602 004056 005024      DBUFCL: CLR (R4)+
603 004060 020427 005720      CMP R4,#DBUF+16
604 004064 001374      BNE DBUFCL
605 004066 010500      MOV R5,R0:
606 004070 004737 004754      JSR PC,OTD
607 004074 000207      RTS PC
608
609
610
611

```

GTO ANGLE
LOAD FOR ANGLE LIST

INSERT SPACES
; GTO TO DISPLACEMENT

Y-SPACING
X-SPACING
MULTIPLYING BY 100-8

DIVIDE Y BY X

LOAD TANGENT ADDRESS
LOOK FOR ANGLE

ABSOLUTE ANGLE-DEGREES
LOAD ANGLE
DIVIDE BY TWO

LOAD FOR OTD

SPECKLEGRAM ANALYSIS SYSTEM

HPCRO VR05-01H 05-NOV-72 02:24 PAGE 1+

```

612 004076 000000
613 004100 012700 007434
614 004104 012701 007634
615 004110 005710
616 004112 100001
617 004114 005410
618 004116 005711
619 004120 100001
620 004122 005411
621 004124 005004
622 004126 011003
623 004130 032703 000001
624 004134 001401
625 004136 061004
626 004140 006310
627 004142 006203
628 004144 001371
629 004146 005005
630 004150 011103
631 004152 032703 000001
632 004156 001401
633 004160 061105
634 004162 006311
635 004164 006203
636 004166 001371
637 004170 060405
638 004172 010520
639 004174 062701 000002
640 004200 020027 007634
641 004204 001341
642 004206 003207
643
644
645
646
647
648
649
650
651 004210 105737 177564
652 004214 100375
653 004216 012037 177566
654 004222 021027 000000
655 004226 001370
656 004230 000207
657
658

RAMP: HALT
RMP: MOV #FFTBUFF,R0;
      MOV #FFTBUFF+200,R1;
SOR1: TST (R0);
      BPL SOR2
      NEG (R0);
      TST (R1);
      BPL SOR3
      NEG (R1);
      CLR R4
SOR3: MOV (R0),R3
      BIT #1,R3
NOTE1: BEQ SOR4
      ADD (R0),R4;
SOR4: BPL (R0)
      ASR R3
      BNE NOTE1
      CLR R5
      MOV (R1),R3
NOTE2: BIT #1,R3
      BEQ SOR5
      ADD (R1),R5;
SOR5: ASL (R1)
      ASR R3
      BNE NOTE2
      ADD R4,R5;
      MOV R5,(R0)+
      ADD #2,R1
      CMP R0,#FFTBUFF+200
      BNE SOR1
      RTS PC

REAL BUFFERS
IMAGINARY BUFFER
IS REAL POSITIVE ?
IF NOT NEGATE
IS IMAGINARY POSITIVE
IF NOT NEGATE

SQUARE REAL PART

SQUARE IMAGINARY PART

ADD REAL AND IMAGINARY

READY TO PRINT
:PRINT

```


SPECKLEGRAM ANALYSIS SYSTEM

MACRO VR05-01H 05-NOV-72 02:24 PAGE 1+

706 004434	011102	MOV (R1),R2;	LOAD SIN
707 004436	013703	MOV XD1ST0,R3;	LOAD XSPACING
708 004442	005000	CLR R0	
709 004444	060200	MULT6: ADD P2,R0;	MULT XSIN ANGLE
710 004446	162703	SUB #1,R3	
711 004452	020327	CMP R3,#0	
712 004456	001372	BNE MULT6	
713 004460	005003	CLR R3	
714 004462	006200	LESSOR:ASR R0 ;	DIVIDE BY 100-8
715 004464	005203	INC R3	
716 004466	020327	CMP R3,#6	
717 004472	001373	BNE LESSOR	
718 004474	012704	MOV #DBUF,R4;	LOAD TO CLEAR
719 004500	005024	CLR (R4)+	
720 004502	020427	DWUPE: CMP R4,DBUF+16	
721 004506	001374	BNE DWUPE	
722 004510	004767	JSR PC.OTD	
723 004514	010207	RTS PC	
724			
725			
726			
727 004516	000000	AFREQ: HALT	
728 004520	005037	FREQ: CLR H1DC	CHECK FOR H1 DC
729 004524	023727	CMP FFTBUF+176,*156;	
730 004532	002003	BGE HOP	
731 004534	012737	MOV #1,H1DC	INITIALIZE FOR HIGHEST FREQUENCY
732 004542	012700	HOP: MOV #FFTEUF+140,R0;	
733 004546	005003	CLR R3	CHECK IF LAST HIGHER
734 004550	022003	SRCH: CMP (R0)+,R3;	
735 004552	003004	BGT HOLD	DONE ?
736 004554	020027	CMP R0,#FFTEUF+174;	
737 004560	003773	BLE SRCH	
738 004562	000426	BR QUIT	CHECK H1DC SET
739 004564	023727	CMP H1DC,*1;	
740 004572	001006	BNE SKIP	
741 004574	162700	SUB #2,R0	
742 004600	022027	CMP (R0)+,*3	
743 004604	003412	BLE QUIT-6	
744 004606	000405	BR VALID	SKIP FREQ SRCH FOR H1DC
745 004610	162700	SKIP: SUB #2,R0;	
746 004614	022027	CMP (R0)+,*10	
747 004620	003404	BLE QUIT-6	
748 004622	162700	SUB #2,R0	
749 004626	010002	MOV R0,R2	
750 004630	012003	MOV (R0)+,R3	
751 004632	020027	CMP R0,#FFTEUF+174	
752 004636	003744	BLE SRCH	

SPECKLEGRAM ANALYSIS SYSTEM

MACRO VR05-01H 05-NOV-72 02:24 PAGE 1+

```

753 004640 005037 005642      CLR NONE
754 004644 000327 000000      CMP R3,#0
755 004650 001003      RNE FOW
756 004652 005237 005642      INC NONE
757 004656 000435      BR OVER
758 004660 002702 000002      FOW : ADD #2,R2;
759 004664 011200      MOV (R2),R0
760 004666 162702 000004      SUB #4,R2
761 004672 021200      CMP (R2),R0
762 004674 003003      BGT MORE
763 004676 012705 000000      MOV #0,R5
764 004702 000402      BR LIST
765 004704 012705 000001      MORE: MOV #1,R5
766 004710 002702 000002      LIST: ADD #2,R2
767 004714 012701 007634      MOV #FFTBUFF+200,R1
768 004720 160201      SUB R2,R1
769 004722 006201      ASR R1
770 004724 012700 005644      MOV #0BUF,R3
771 004730 010120      MOV R1,(R0)+
772 004732 020527 000001      CMP R5,#1
773 004736 001003      RNE LESS
774 004740 012710 000053      MOV #53,(R0)
775 004744 000402      BR OVER
776 004746 012710 000055      LESS: MOV #55,(R0)
777 004752 000207      OVER: RTS PC
778
779
780
781
782
783
784
785 004754 012701 005702      OTD: MOV #0BUF,R1
786 004760 005002      CLR R2
787 004762 020927 023420      CMP R0,#23420;
788 004766 002405      BLT .+14      10000.
789 004770 162700 023420      SUC #23420,R0
790 004774 062702 000001      ADD #1,R2
791 004776 000770      BR .-16
792 005000 002702 000060      ADD #60,R2;
793 005002 010221      MOV R2,(R1)+
794 005006 005002      CLR R2
795 005010 020027 001750      CMP R0,#1750;
796 005012 002405      BLT .+14      1000.
797 005016 162700 001750      SUC #1750,R0
798 005020 062702 000001      ADD #1,R2

```

SPECKLEGRAM ANALYSIS SYSTEM

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800 005030	000770	BR -16	
801 005032	062702	ADD #60.R2;	ASCII
802 005036	010221	MOV R2.(R1)+	
803 005040	005002	CLR R2	
804 005042	020027	CHP R0.#144	
805 005046	002405	BLT +14	100.
806 005050	162700	SUB #144.R0;	
807 005054	062702	ADD #1.R2	
808 005060	000770	BR -16	ASCII
809 005062	062702	ADD #60.R2;	
810 005066	010221	MOV R2.(R1)+	
811 005070	005002	CLR R2	
812 005072	030027	CHP R0.#12	
813 005076	002405	BLT +14	10.
814 005100	162700	SUB #12.R0;	
815 005104	062702	ADD #1.R2	ASCII
816 005110	000770	BR -16	
817 005112	062702	ADD #60.R2;	
818 005116	010221	MOV R2.(R1)+	
819 005120	005002	CLR R2	LSD
820 005122	062700	ADD #60.R0;	LOAD TO DBUF
821 005126	010021	MOV R0.(R1)+;	
822 005130	000207	RTS PC	
823			
824			
825			
826			
827 005132	000000	ASTAGE:HALT	
828 005134	005037	STAGE: CLR COLM	
829 005140	005037	CLR LINE	
830 005144	005037	CLR UNIT	
831 005150	005037	CLR DELAY	
832 005154	012737	XSTEP: MOV #1.#164000;	KEEP TRACK
833 005162	062737	ADD #1.UNIT;	
834 005170	062737	ADD #1.LINE	DELAY
835 005176	005237	INC DELAY;	
836 005202	023727	CHP DELAY.#100	
837 005210	001372	BIE XLOOP	
838 005212	005037	CLR DELAY	
839 005216	023737	CHP UNIT.STEPX;	DONE INC SCAN ?
840 005224	001353	BIE XSTEP	
841 005226	005037	CLR UNIT	
842 005232	004737	JSR PC.POSITN;	GTO POSITN
843 005236	004737	JSR PC.MANIP;	GTO MANIP
844 005242	005037	CLR RATHER	
845 005246	013737	MOV XLINIT.UNIT	
846 005254	023737	CHP LINE.UNIT;	DONE LINE SCAN ?

PECKLEGRAM ANALYSIS SYSTEM

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847 005262	100730	BMI XSTEP-10	Y-STAGE PULSE
848 005264	000443	BR ZEROX	KEEP TRACK
849 005266	012737	YSTEP: MOV #2.0#164000;	
850 005274	062737	ADD #1.0#164000;	
851 005302	052737	ADD #1.0#164000;	
852 005310	005237	YLOOP: INC UNIT	
853 005314	023727	CIP UNIT.#100;	
854 005322	001372	BNE YLOOP	
855 005324	005037	CLR UNIT	
856 005330	023737	CIP DELAY. STEP;	
857 005336	001353	BNE YSTEP	
858 005340	004737	JSR PC.POSITN	
859 005344	004737	JSR PC.POSITN	
860 005350	005037	CLR RATHER	
861 005354	013737	MOV YLINIT.UNIT;	
862 005362	023737	CIP COLN.UNIT	
863 005370	003665	BLE XSTEP-10	
864 005372	000207	RTS PC	
865 005374	012737	ZEROX: MOV #1.0#164000;	
866 005382	012737	XZERO: MOV #1.0#164000;	
867 005410	162737	SUB #1.LINE	
868 005416	005237	DOLoop: INC UNIT	
869 005422	023727	CIP UNIT.#100;	
870 005430	001372	BNE DOLoop	
871 005432	005037	CLR UNIT	
872 005436	023727	CIP LINE.#0;	
873 005444	001356	BNE XZERO	
874 005446	005237	ROUND: INC UNIT	
875 005452	023727	CIP UNIT.#40000;	
876 005460	001372	BNE ROUND	
877 005462	005037	CLR UNIT	
878 005466	005037	CLR DELAY	
879 005472	012737	MOV #4.0#164000;	
880 005500	000672	BR YSTEP	
881			
882			
883 005502	012700	POSITN: MOV #DEUF.R0;	
884 005506	005020	DCLEAR: CLR (R0)+	
885 005510	020027	CIP R0.#DBUF+12;	
886 005514	001374	BNE DCLEAR	
887 005516	013700	MOV LINE.R0;	
888 005522	004737	JSR PC.OTD;	
889 005526	012700	MOV #DBUF.R0	
890 005532	004737	JSR PC.TTYOUT;	
891 005536	013700	MOV COLN.R0;	
892 005542	004737	JSR PC.OTD;	
893 005546	012700	MOV #SPC.R0	

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0 FOR X, 1 FOR Y

SPECKLEGRAM ANALYSIS SYSTEM

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937 005754	000000	RATIO: .WORD 0			
938 005756	000000	RUBUF: .WORD 0.0			
939 005762	000000	MEAN: .WORD 0.0,0.0,0.0,0.0			
940 005770	000000	XLIMIT: .WORD 0.0,0.0,0.0,0.0			
941 005812	000000	YLIMIT: .WORD 0.0,0.0,0.0,0.0			
942 005826	000000	INX: .WORD 0.0,0.0,0.0,0.0			
943 005842	000000	INCY: .WORD 0.0,0.0,0.0,0.0			
944 005856	000000	STEPX: .WORD 0			
945 005860	000000	STEPI: .WORD 0			
946 005862	000015	ASKAV: .WORD 15,12,12			
947 005870	000117	.WORD 116,117,56,43,40,104;			NO. * DATA AVERAGES
948 005876	000043	.WORD 101,124,101,40,101,126			
949 005884	000101	.WORD 105,122,101,107,105			
950 005892	000105	.WORD 123,40,54,40,0			
951 005900	000123	XDIST: .WORD 15,12,12			
952 005908	000130	.WORD 130,55,124,117,124;			X-TOT SCAN DISTANCE
953 005916	000137	.WORD 40,123,103,101,116			
954 005924	000140	.WORD 40,104,111,123,124			
955 005932	000143	.WORD 101,116,103,105,40			
956 005940	000146	.WORD 77,40,54,40,0			
957 005948	000149	YDIST: .WORD 15,12,12			
958 005956	000152	.WORD 131,55,124,117,124;			Y-TOT SCAN DISTANCE
959 005964	000155	.WORD 40,123,103,101,116			
960 005972	000158	.WORD 40,104,111,123,124			
961 005980	000161	.WORD 101,116,103,105,40			
962 005988	000164	.WORD 77,40,54,40,0			
963 005996	000167	XINC: .WORD 15,12,12			
964 006004	000170	.WORD 130,55,111,116,103;			X-INCREMENT

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SPECKLEGRAM ANALYSIS SYSTEM

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SYMBOL TABLE

A	005630	ARIP	004076	ARANGE	003760
ADISP	004424	AD0	001506	AFET	001462
AFREQ	004516	AG1	002304	AG2	002324
AG3	002366	ALORD	002626	ALOOP	003552
ALPHA	001706	AKNIP	001246	AKP	004100
ANGLE	003762	APRINT	003640	AREAD	003216
ASC11	001034	ASKAV	006062	ASTAGE	005132
AVER	003372	AZERO	002154	B	005632
B10	001510	BEGIN	003060	BETA	001736
BZERO	002314	C	005634	C10	001606
CHECK	002454	C1PCLE	003622	CLEAR	000562
CLOCK1	003224	CLOCK2	003300	CLOCK3	003330
CLOCK4	003344	CLOCK5	003436	CLP1	001254
CLR2	001220	CLST	001236	COLM	005730
COS	010674	CYCLES	006772	CZERO	002576
D	003052	DATH	010046	D8UF	005702
DEUFCL	004056	DCLEAR	005506	DELAY	005726
DIVANG	004050	DINFEAD	003516	DOCTR	004010
DLOOOP	005416	DOHE1	003240	DOHE2	003360
DOHE3	003452	DOT	002556	DOWN	001576
DROP	001572	DUPPED	003566	DWIPE	004500
DZERO	002442	EAT	002516	ECHO	004340
EOL	006756	E1	004374	FBUFFAV	007022
FFT	001464	FFTBUFF	007434	FIN	006460
FLG	005664	FOW	004660	FOWARD	003602
FREQ	004520	FUD1	002214	FUD2	002334
FUD3	002464	FUD4	002636	FUNC	005650
F3	001452	F4	001442	GAHA	001776
GOOF	006444	GOON	002174	GOOHY	002616
HEAD	006576	H1DC	005734	HIGH	002566
HOLD	004564	HOP	004542	HURPS	001356
INCH	006026	INCY	006042	INPUT	004320
JUG	002246	JUGGER	002670	JUMP	000556
KBB	177562	KBS	177560	KEEP	005666
KILL	001714	LESS	004746	LESSOR	004462
LINE	005724	L1ST	004710	L1FD	004406
LOAD	002204	LOOKUP	004030	LOOP1	003426
LOOP2	003510	LOW	002510	L10.	002752
L11.	002766	L12.	003016	L3	001770
L5	002026	L6	002074	L7	002374
L8.	002674	L9.	002724	MAHIP	001250
MEAN	005762	MINUS	002166	MORE	004704
MULT1	003774	MULT4	002432	MULT6	004444
NOLIST	001376	NOME	005642	NORMAL	001474
NOTE1	004130	NOTE2	004152	N1	004246
N2	004262	N3	004276	N4	004312
OBUF	005644	OPER	004232	OTD	004754

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SPECKLEGRAM ANALYSIS SYSTEM

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SYMBOL TABLE

OTHER	002134	OVER	004752	PC	=2000007
PLUS	002144	POSITN	005502	PRINT	003642
QUES	010100	QUIT	004640	RATHER	005746
RATIO	005754	FEAD	003220	RECLR	003176
ROBUF	005756	ROUND	005446	PR0	005604
RR1	005606	RR2	005610	RR3	005612
RR4	005614	RR5	005616	RR6	005620
RR7	005622	RR8	005624	RR9	005626
RR	=2000000	R1	=2000001	R2	=2000002
R3	=2000003	R4	=2000004	R5	=2000005
SECOND	005640	CEE	001544	SHIFT	001680
SIN	011000	SINBUF	010422	SKIP	004610
SLIDE	003120	SLIP	001616	SLOW	003316
SP	=2000006	SFC	006742	SOCZ	005732
SOR1	004110	SOR2	004116	SOR3	004124
SOR4	004140	SOR5	004162	SRCH	004550
STAGE	005134	START	000500	STEPX	006056
STERY	005060	STORE	001502	TANBUF	010134
TEST	003112	TINES	005744	TFR	=177566
TPS	=177564	TSACK	005742	TYOUT	004310
UNIT	005722	UP	001552	VALID	004622
UNIT	003276	WHICH	005740	X	005636
XDIST	006144	XDISTO	005750	XINC	006324
XLIMIT	005776	XLOOP	005176	XREAD	005736
XSTEP	005154	XZERO	005402	YDIST	006234
YDISTO	005752	YINC	006374	YLIMIT	006012
YLOOP	005310	YSTEP	005266	ZEROX	005374
. ABS.	011102		000		
	000000		001		

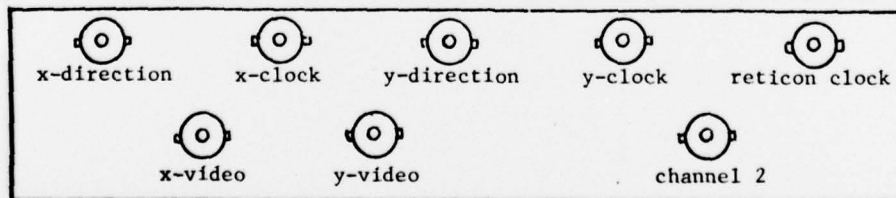
ERRORS DETECTED: 0
FREE CORE: 4851. WORDS
DC:RL.OBJ.LP:LIST<DT1:RL.SRC

APPENDIX III

SYSTEM OPERATING INSTRUCTION

OPERATING PROCEDURES:

- I. The initial set-up should be performed as follows:
 1. A 15 milliwatt or greater He-Ne laser should be aligned on the centerline of an optical bench, 8.75 inch above the surface of the bench, with all of the optics centered on this beam.
 2. Set up the beam-reducing optics as described in the Optical Setup Section of this report and insert an optical attenuator immediately following these optics.
 3. Place the x-y stage as close to the attenuator as needed.
 4. Align a ground glass screen, with a D.C. spot block, so that the D.C. component of the fringe halo image falls on the block. Position the ground glass in the optical axis direction so that a fringe halo of 2-4 inches in diameter exists.
 5. An imaging lens ($f=28\text{mm}$) should be centered on the optical axis and positioned to image the fringe pattern onto the detectors. The distances between the lens and the detector all depend upon the image aperture of the specklegram recording system. Essentially for the fringe spacing of a given specklegram to be analyzed accurately, the readout halo size depends on the recording aperture.
 6. Connect the x-y stage cables to the appropriate x-y Aerotek Drive Units via the 8 pin connector plugs.
 7. A labeled BNC wiring panel is attached to the top back of the rack mounting cart and is illustrated below.



A list of to and from BNC connections are shown in the following table:

WIRING DIAGRAM	
FROM	TO
Aerotek Drive-(x) DIR	Panel - x - direction
Aerotek Drive-(x) CL	Panel - x - clock
Aerotek Drive-(y) DIR	Panel - y - direction
Aerotek Drive-(y) CL	Panel - y - clock
Reticon -x video	Panel - x - video
Reticon -y video	Panel - y - video
Reticon -Ext. clock	Panel - reticon clock
Reticon -EOS	Panel - channel 2

8. AC connections from the Aerotek Drive Units, PDP 11 computer, off-on indicator light, and control electronics panels should be plugged into the AC terminal strip in the lower rear of the rack mounting cart.

9. Connect the teletype I/O to the computer I/O cable and plug the teletype into a wall socket.

10. Turn on all equipment and check out this equipment with a test paper tape given to you by AFAL/DHO-2.

II. AFTER CHECK-OUT (Initializing for a read sequence)

1. Place Specklegram into 4 inch by 5 inch holder.
2. Align the readout beam to the upper right hand corner of the specklegram plate, (facing the plate), by setting the local-remote switch on the x drive unit to the local position and pushing the slew button until the upper right hand x position is reached. The + or - switch will be set according to the initial position of the plate before setting up. The slew speed can also be changed by the small potentiometer on the front panel. Repeat for the y-position.
3. Reset the x and y digital display to zero by depressing the reset button and switch the remote-local switches to the remote position. The system is now ready for computer control operation.

4. Load the control program through the paper tape reader on the teletype by the following procedure:

A.) If the Bootstrap loader is not contained in core-memory, a hand loading procedure is as follows:

a.) Toggle in 017744 onto the computer switches and hit LOAD ADDR Button.

b.) Toggle 016701 and hit the DEP button and continue DEP operations on these numbers: 000026, 012702, 000352, 005211, 105711, 100376, 116162, 000002, 017400, 005267, 177756, 000765, 177560, 000000.

B.) Set the ABSOLUTE LOADER paper tape into the reader with the leader section in the reader section, and set the reader switch to the top position called START.

C.) 017744 and LOAD ADDR then START. The Absolute loader should now pass through the reader and stop when finished.

D.) Load the Control tape into the reader with the leader positioned in the reader section, and set the read switch up.

E.) 017500 and LOAD ADDR then START. The control tape should now pass through the reader and stop when finished. The control program is now loaded.

5. Make sure all connections are made and all power switches are activated. The program is now ready to run.

6. 000500 and LOAD ADDR, then START.

7. The teletype will now ask initializing questions before displaying specklegram data and these questions can be answered as described in the Software Section of this report. When the data run is finished, the teletype will print "SCAN COMPLETED".

8. If, before shutdown, another plate is to be analyzed, only the following steps have to be repeated:

II. - 1,2,3,6

9. The computer can be stopped during any phase of operation by simply hitting the HALT Button and after a data run there is no specific shutdown sequence except that the HALT button should be activated before shutting any other power off.

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10. Once the procedures of Sections I and II of the operating procedures have been performed complete, only steps II. - 1, 2, 3, 4B, 4C, 4D, 4E, 5, and 6 have to be repeated.

APPENDIX IV

A TYPICAL SPECKLEGRAM EXPOSURE AND READOUT

Appendix V is designed to inform the reader in brief of a typical experiment run through from initial exposure to final readout, with the understanding that specific details can be obtained from the references listed at the end of the report.

1. EXPOSURE

In recording speckelgram data, if the laser has a wavelength of 5140 angstroms and the lens has an f-number equal to 2, then the speckle size projected onto the film plane is approximately 1 micrometer, which is defined as the minimum speckle size for our purposes. This minimum sets one parameter related to the system resolution. The next question related to the system resolution is what is the maximum and minimum shift that can be tolerated? Sampling Theory requires that the shift be greater than 2 speckle sizes (2 micrometers). The maximum shift is defined by requiring the shift not to be larger than the readout beam size (.5 to 1 millimeter). The reason for this maximum is that the surface across the reading aperture can be shifted in only one direction with the randomness of the speckle remaining unchanged. The exposure time required on the film plane is proportional to the film sensitivity and for a typical film (Kodak 649-F), 500 ergs/cm^2 is needed. Assuming now for simplicity a square centimeter of gray steel (55% reflectivity) as a specimen, a 50 milliwatt laser as an illuminator source, in which all of the light intercepts the 1 cm^2 area, and a cosine reflection distribution from the specimen with 1% of the reflected light reaching the imaging lens, a typical exposure might be as follows:

$$\begin{aligned} 1000 \text{ ergs} &= 10^{-4} \text{ watt-sec} \\ 500 \text{ ergs} &= .05 \text{ milliwatt-sec} \\ .05/50/.55/.01 &= .18 \text{ seconds} \end{aligned}$$

The .18 second exposure time assumes ideal conditions, thus optical losses in the system would require more exposure time.

The processing required is the standard film process:

1. Develop (D-19) - 6 minutes
2. Stop (Stop Bath) -30 seconds
3. Fix (Rapid Fixer) - 5 minutes

The plate is now ready for readout.

2. READOUT

Readout techniques used for extracting the fringe information from a specklegram and a typical fringe halo are, for the purposes of this report, as follows. A 1 mm readout beam diameter is chosen, thus providing a maximum of 13000 data points on one 4 inch by 5 inch film plate. Since the readout procedure for each point is the same, the procedure for only one point will be discussed. The halo containing the fringe information is defined as a conical ray of light diverging from the center of the readout beam with a cone angle directly calculatable from the recorded speckle size as follows:

$$2\lambda/D = \theta$$

where D=the speckle size. If D=1 micrometer and $\lambda = .5$ micrometer, then $\theta = 1$ radian.

Since the recording speckles are arranged in a random fashion and the speckle shift is in only one direction over the area defined by a 1 mm aperture, then the analogy can be made that the random speckle shift acts similarly to a double slit optical configuration.

The equation for the double slit is

$$n\lambda = 2d \sin \theta$$

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where n is the order of the fringe, λ is the wavelength of light, d is the distance between slits (or speckle correlation shift) and θ the angle of the fringe transmission.

This says that the first dark fringe should be located at an angle of

$$\theta = \lambda/2d$$

if θ is a small angle.

It should be obvious at this point that the specklegram strain analysis technique is an excellent tool for looking at in-plane displacements or strains parrallel to the recording surface, while holographic interferometry best applied to out-of-plane measurements; thus the two techniques should complement each other for solving many strain and stress problems existent in the Air Force.

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